

Hugo Hens

Performance Based Building Design 2

From Timber-framed Construction to Partition Walls



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To my wife, children and grandchildren

In remembrance of Professor A. de Grave who introduced building physics as a new discipline at the University of Leuven, KULeuven, Belgium, in 1952

Preface

Overview

Just like building physics, performance based building design was hardly an issue before the energy crises of the 1970s. With the need to upgrade energy efficiency, the interest in overall building performance grew. The volume on applied building physics discussed a performance rationale and performance requirements at the building and building enclosure level, with emphasis on heat, air, moisture checks. As in the third volume, volume four continues this rationale for structural aspects, acoustics, fire safety, maintenance and buildability. And as with volume three, it is the result of thirty-eight years of teaching architectural, building and civil engineers, coupled to more than forty years of experience in research and consultancy. Where and when needed, input and literature from around the world has been used, with a list of references and literature at the end of each chapter.

The book can be used by undergraduates and graduates in architectural and building engineering and also building engineers who want to refresh their knowledge may also benefit. The level of discussion assumes a sound knowledge of building physics, along with a background in structural engineering, building materials and building construction.

Acknowledgements

A book of this magnitude reflects the work of many, not only the author. Therefore, first of all, we want to thank our thousands of students. They gave us the opportunity to test the content and helped in upgrading by the corrections they proposed and the experience they offered in learning what parts should be better explained.

This is a text that has been written standing on the shoulders of those who came before us. Although we started our career as a structural engineer, our predecessor, Professor Antoine de Grave planted the seeds from which our interest in building physics, building services and performance based building design slowly grew. The late Bob Vos of TNO, the Netherlands, and Helmut Künzel of the Fraunhofer Institut für Bauphysik, Germany, showed the importance of experimental work and field testing for understanding building performance, while Lars Erik Nevander of Lund University, Sweden, taught that application does not always ask extended modeling, mainly because reality in building construction is much more complex than any simulation is.

During the four decades at the Laboratory of Building Physics, several researchers and Ph. D.-students got involved. I am very grateful to Gerrit Vermeir, Staf Roels, Dirk Saelens and Hans Janssen who became colleagues at the university; to Jan Carmeliet, now professor at the ETH-Zürich; Piet Standaert, a principal at Physibel Engineering; Jan Lecompte, at Bekaert NV; Filip Descamps, a principal at Daidalos Engineering and part-time professor at the Free University Brussels (VUB); Arnold Janssens, professor at the University of Ghent (UG); Rongjin Zheng, associate professor at Zhejiang University, China, and Bert Blocken, professor at the Technical University Eindhoven (TU/e), who all contributed by their work. The experiences gained by working as a structural engineer and building site supervisor at the start of my career, as building assessor over the years, as researcher and operating agent of four Annexes of the IEA, Executive Committee on Energy Conservation in Buildings and Community Systems, forced me to rethink the engineering based performance approach each time again. The many ideas I exchanged with Kumar Kumaran, Paul Fazio, Bill Brown,

VIII Preface

William B. Rose, Joe Lstiburek and Anton Ten Wolde in Canada and the USA were also of great help. A number of reviewers took time to examine the book. Although we do not know their names, we also thank them here.

Finally, I thank my family, my wife Lieve, who managed living together with a busy engineering professor, my three children who had to live with that busy father and my many grandchildren who do not know their grandfather is still busy.

Leuven, June 2012

Hugo S. L. C. Hens

Contents

	Preface	VII
0	Introduction	. 1
0.1	Subject of the book.	. 1
0.2	Units and symbols	. 1
0.3	References and literature	. 5
1	Timber-framed construction	. 7
1.1	In general	. 7
1.2 1.2.1 1.2.2 1.2.2.1 1.2.2.2 1.2.2.3 1.2.2.4 1.2.2.5 1.2.3 1.2.4 1.2.5 1.2.6	Performance evaluation Structural integrity Building physics: heat, air, moisture Air tightness Thermal transmittance Transient response Moisture tolerance Thermal bridges Building physics: acoustics Durability Fire safety. Maintenance	. 9 11 13 16 17 23 24 24 25
1.3 1.3.1 1.3.2 1.3.3 1.3.4 1.3.5 1.3.6	Design and execution Above grade Frame Thermal insulation Air and vapour retarder Building paper Variants.	25 26 26 26 26 27
1.4	References and literature	27
2	Sheet-metal outer wall systems	31
2.1	In general	31
2.2 2.2.1 2.2.2 2.2.2.1 2.2.2.2 2.2.2.3 2.2.2.4 2.2.2.5	Performance evaluation Structural integrity Building physics: heat, air, moisture Air tightness Thermal transmittance Transient response Moisture tolerance Thermal bridges	31 32 32 33 33

X Contents

2.2.3 2.2.4 2.2.5 2.2.6	Building physics: acoustics Durability Fire safety Maintenance	36 36
2.3	Design and execution	36
2.4	References and literature	37
3	New developments	39
3.1 3.1.1 3.1.2 3.1.2.1 3.1.2.2	Transparent insulation In general Performance evaluation Building physics: heat, air, moisture Durability	39 39 39
3.2	Multiple skin and photovoltaic outer walls	44
3.3	References and literature	44
4	Roofs: requirements	45
4.1	In general	45
4.2 4.2.1 4.2.2 4.2.2.1 4.2.2.2 4.2.2.3 4.2.2.4 4.2.2.5 4.2.3 4.2.4 4.2.5 4.2.6 4.3	Performance evaluation Structural integrity Building physics: heat, air, moisture Air tightness Thermal transmittance Transient response Moisture tolerance Thermal bridges Building physics: acoustics Durability Fire safety Maintenance and economy References and literature	45 45 45 46 47 48 48 49 49
5	Low-sloped roofs	51
5.1	Typologies	51
5.2 5.2.1.1 5.2.1.2 5.2.1.3 5.2.1.4 5.2.1.5 5.2.2 5.2.3	Roofing membranes Build-up, multi-ply roofing Number of layers Execution Bonding Protection Combination with the type of substrate Build up polymer roofing. Problems with roofing	53 54 54 55 55 56 56
5.2.3.1	Pimples	56

Contents XI

5.2.3.2 5.2.3.3 5.2.3.4	Alligator skin	57
5.3 5.3.1.1 5.3.1.2 5.3.1.3 5.3.1.4 5.3.2 5.3.2.1 5.3.2.2 5.3.2.3 5.3.2.4 5.3.2.5 5.3.3.1 5.3.3.2 5.3.3.3.1	Compact low-sloped roofs Assemblies Heavy deck Semi-heavy deck Light-weight deck Conclusion Performance evaluation Structural integrity Building physics: heat, air, moisture Building physics: acoustics Fire safety Maintenance Design and execution Assembly Details Special low-sloped roof uses	58 59 59 60 62 81 81 81 81 82
5.4 5.4.1 5.4.2 5.4.2.1 5.4.2.2 5.4.2.3 5.4.3.1 5.4.3.2 5.4.3.3	Protected membrane roofs In general Performance evaluation Thermal transmittance Moisture tolerance Other performances Design and execution Roofing membrane Details Globally References and literature	85 86 90 92 92 92 93 93
6	Pitched roofs	97
6.1 6.1.1 6.1.1.1 6.1.1.2 6.1.2.1 6.1.2.2 6.1.2.3 6.1.3	Classification Type of form. Simple roofs Composite roofs Type of supporting structure Purlins Rafters Other. Type of cover	97 97 98 98
6.2 6.2.1 6.2.1.1 6.2.1.2 6.2.1.3		99 99 99 101 102

XII Contents

6.2.2 6.2.2.1 6.2.2.2 6.2.2.3 6.2.3 6.2.4	Fibre cement. Timber slates and plain tiles. Corrugated sheets.	102 103 103 104 104
6.3	Basic assemblies.	105
6.4 6.4.1 6.4.2 6.4.2.1 6.4.2.2 6.4.2.3 6.4.2.4 6.4.2.5 6.4.3 6.4.4 6.4.5 6.4.6	Structural integrity Building physics: heat, air, moisture Air tightness Thermal transmittance Transient response Moisture tolerance Thermal bridges Building physics: acoustics Durability Fire safety Maintenance	141 141 142 142
6.5 6.5.1 6.5.1.1 6.5.1.2 6.5.2	Design and execution Roof assemblies Attic as storage and buffer space Inhabited attic Roof details	143 143
6.6	References and literature	149
7	Sheet-metal roofs	153
7.1	In general	153
7.2 7.2.1 7.2.2 7.2.3 7.2.4 7.2.5	Lead Copper and brass Zinc	154 156
7.3 7.3.1 7.3.1.1 7.3.1.2 7.3.1.3 7.3.1.4 7.3.2 7.3.3	Performance evaluation Moisture tolerance In general Lack of air tightness Under cooling. Two practice and six test building cases Thermal bridges Durability	159
7.4	Design and execution	170
7.5	References and literature	170

Contents XIII

8	Windows, outer doors and glass façades	173
8.1	In general	173
8.2 8.2.1 8.2.2 8.2.2.1 8.2.2.2 8.2.2.3 8.2.2.4 8.2.2.5 8.2.2.6 8.2.2.7 8.2.3	Glass In general Performance evaluation Structural safety Building physics: heat, air, moisture Building physics: acoustics Building physics: light Durability Fire safety Break-in safety Technology	173 174 174 177 194 196 197 198
8.3 8.3.1 8.3.2 8.3.2.1 8.3.2.2 8.3.2.3 8.3.2.4 8.3.2.5 8.3.2.6 8.3.3 8.3.3.1 8.3.3.2 8.3.3.3	Windows and doors In general Performance evaluation Structural safety Building physics: heat, air, moisture Building physics: acoustics Durability Fire safety Maintenance and safety at use Technology Timber, vinyl Aluminium, steel Window blinds and roller shutters Trickle vents	200 204 204 210 211 211 212 212 212 212
8.4 8.4.1 8.4.2 8.4.3 8.4.4 8.4.5 8.4.5.1 8.4.5.2 8.4.5.3 8.4.5.4 8.4.5.5 8.4.6	Glass façades In general Window fronts Curtain walls Structural and suspended glazing. Double skin façades In general Building physics: heat, air, moisture Building physics: acoustics Fire safety. Building level: energy efficiency Photovoltaic façades (PV) References and literature	214 214 215 217 218 218 225 226 226 226
9	Balconies, shafts, chimneys and stairs	231
9.1	In general	231
9.1 9.2 9.2.1	Balconies In general	231

XIV Contents

9.2.2	Performance evaluation	231
9.2.2.1	Structural integrity	231
9.2.2.2	Building physics: heat, air, moisture	
9.2.2.3	Durability	
9.2.2.4	Fire safety	
9.2.2.5	User's safety	
9.2.3	Design and execution	
9.2.3.1	Thermal cuts	
9.2.3.2	Water proofing and drainage	
9.2.3.3	Floor finish.	
9.2.3.4	Hand rails	
9.3	Shafts	
9.3.1	In general	235
9.3.2	Performance evaluation	235
9.3.2.1	Structural integrity	236
9.3.2.2	Building physics	236
9.3.2.3	Fire safety	236
9.3.3	Design and execution	
9.4	Chimneys	237
9.4.1	In general	
9.4.2	Design considerations	237
9.4.3	Design and execution	
9.4.3.1	Stoves	
9.4.3.2	Boilers	239
9.5	Stairs	240
9.5.1	In general	
9.5.1	Performance evaluation	240
9.5.2.1	Structural integrity	
9.5.2.1	Building physics: acoustics	
9.5.2.2	Fire safety.	_
9.5.2.3 9.5.2.4	User's safety.	
9.5.2.4 9.5.3		
9.3.3	Design and execution	244
9.6	References and literature	244
10	Partitions; wall, floor and ceiling finishes; inside carpentry	245
10.1		245
10.1	Overview	245
10.2	Partition walls.	245
10.2.1	In general	245
10.2.2	Performance evaluation	
	Structural integrity	
	Building physics: heat, air, moisture	
	Building physics: acoustics	
	Durability	
	Fire safety.	
10.2.3	Design and execution	
		ムコノ

Contents XV

10.3	Building services	250
10.4.2.2 10.4.2.3 10.4.2.4 10.4.3 10.4.3.1	Wall finishes In general Performance evaluation Structural integrity Building physics: heat, air, moisture Building physics: acoustics Fire safety Design and execution Wet plasters Gypsum board	250 250 250 251 251 251 251 251
$10.5.2.2 \\ 10.5.2.3$	Floor finishes In general Performance evaluation Structural integrity Building physics: heat, air, moisture Building physics: acoustics Durability Design and execution	252 253 253 254 255 256
10.6.2.2 10.6.2.3 10.6.2.4	Ceiling finishes In general Performance evaluation Structural integrity Building physics: heat, air, moisture Building physics: acoustics Fire safety Design and execution	258 258 258 259 259
10.7.2.2 10.7.2.3 10.7.2.4	Inside carpentry In general Performance evaluation Structural integrity Building physics: heat, air, moisture Building physics: acoustics Fire safety Design and execution References and literature	260 260 260 261 261 262
11	Risk analysis	265
11.1	In general	265
11.2	Risk definition	265
11.3 11.3.1 11.3.2 11.3.3	Performing a risk analysis Identification and probability of deficiencies Severity of the consequences Proposals to limit risks	266 266 266 266

Contents
(

11.4	Example of risk analysis: cavity walls	267
11.4.1	Generalities	267
11.4.2	Deficiencies encountered	267
11.4.3	Probabilities	269
11.4.4	Severity of the consequences	269
11.4.5	Risk?	271
11.4.5.1	Mould	271
	Rain penetration	
	Others	
	Evaluation	
11.4.7	Upgrade proposals	274
11.5	References and literature	274

0 Introduction

0.1 Subject of the book

This is the second part of the third volume in a series of books on building physics, applied building physics and performance based building design:

- Building Physics: Heat, Air and Moisture
- Applied Building Physics: Boundary Conditions, Building Performance and Material Properties
- Performance Based Building Design 1
- Performance Based Building Design 2

Performance Based Building Design 2 continues the application of the performance based engineering rationale, discussed in 'Applied Building Physics: Boundary Conditions, Building Performance and Material Properties' to the design and construction of building assemblies. In order to do that, the text considers the performance requirements presumed or imposed, their prediction during the design stage and the technology needed for realization.

Performance Based Building Design 1 ended with massive outer walls. Performance Based Building Design 2 begins with lightweight building and outer wall systems: timber-framed and metal-based. Then low-sloped, pitched, and metal roofs follow to finish the enclosure-related subjects with glazed surfaces and windows. Attention then turns to balconies, chimneys, shafts, staircases, inside partitions, and finishes. The volume closes with a chapter on risk analysis. Of course, for principals acceptable risk is an important issue. As in Performance Based Building Design 1, the impact of performance requirements on design and execution is highlighted. For decades, the Laboratory of Building Physics at the KULeuven not only tested highly insulated massive façade assemblies, but also lightweight façade assemblies and roofs. The results are used in the discussions.

0.2 Units and symbols

The book uses the SI-system (internationally mandatory since 1977). Base units are the meter (m), the kilogram (kg), the second (s), the Kelvin (K), the ampere (A) and the candela. Derived units of importance are:

```
Unit of force: Newton (N); 1 \text{ N} = 1 \text{ kg} \cdot \text{m} \cdot \text{s}^{-2}

Unit of pressure: Pascal (Pa); 1 \text{ Pa} = 1 \text{ N/m}^2 = 1 \text{ kg} \cdot \text{m}^{-1} \cdot \text{s}^{-2}

Unit of energy: Joule (J); 1 \text{ J} = 1 \text{ N} \cdot \text{m} = 1 \text{ kg} \cdot \text{m}^2 \cdot \text{s}^{-2}

Unit of power: Watt (W); 1 \text{ W} = 1 \text{ J} \cdot \text{s}^{-1} = 1 \text{ kg} \cdot \text{m}^2 \cdot \text{s}^{-3}
```

For the symbols, the ISO-standards (International Standardization Organization) are followed. If a quantity is not included in these standards, the CIB-W40 recommendations (International Council for Building Research, Studies, and Documentation, Working Group 'Heat and Moisture Transfer in Buildings') and the list edited by Annex 24 of the IEA, ECBCS (International Energy Agency, Executive Committee on Energy Conservation in Buildings and Community Systems) are applied.

2 0 Introduction

Table 0.1. List with symbols and quantities.

Symbol	Meaning	Units
a	Acceleration	m/s ²
а	Thermal diffusivity	m^2/s
b	Thermal effusivity	$W/(m^2\cdot K\cdot s^{0.5})$
c	Specific heat capacity	$J/(kg \cdot K)$
c	Concentration	kg/m^3 , g/m^3
e	Emissivity	_
f	Specific free energy	J/kg
	Temperature ratio	-
g	Specific free enthalpy	J/kg
g	Acceleration by gravity	m/s^2
g	Mass flow rate, mass flux	$kg/(m^2 \cdot s)$
h	Height	m
h	Specific enthalpy	J/kg
h	Surface film coefficient for heat transfer	$W/(m^2 \cdot K)$
k	Mass related permeability (mass may be moisture, air, salt)	S
l	Length	m
l	Specific enthalpy of evaporation or melting	J/kg
m	Mass	kg
n	Ventilation rate	s^{-1}, h^{-1}
p	Partial pressure	Pa
q	Heat flow rate, heat flux	W/m^2
r	Radius	m
S	Specific entropy	$J/(kg \cdot K)$
t	Time	S
и	Specific latent energy	J/kg
v	Velocity	m/s
w	Moisture content	kg/m ³
x, y, z	Cartesian co-ordinates	m
A	Water sorption coefficient	$kg/(m^2 \cdot s^{0.5})$
A	Area	m^2
В	Water penetration coefficient	m/s ^{0.5}
D	Diffusion coefficient	m^2/s
D	Moisture diffusivity	m^2/s
E	Irradiation	W/m ²

Table 0.1. (continued)

Symbol	Meaning	Units		
\overline{F}	Free energy	J		
G	Free enthalpy	J		
G	Mass flow (mass = vapour, water, air, salt)	kg/s		
Н	Enthalpy	J		
I	Radiation intensity	J/rad		
K	Thermal moisture diffusion coefficient	$kg/(m \cdot s \cdot K)$		
K	Mass permeance	s/m		
K	Force	N		
L	Luminosity	W/m^2		
M	Emittance	W/m^2		
P	Power	W		
P	Thermal permeance	$W/(m^2 \cdot K)$		
P	Total pressure	Pa		
Q	Heat	J		
R	Thermal resistance	$m^2 \cdot K/W$		
R	Gas constant	J/(kg·K)		
S	Entropy, saturation degree	J/K, –		
T	Absolute temperature	K		
T	Period (of a vibration or a wave)	s, days, etc.		
U	Latent energy	J		
U	Thermal transmittance	$W/(m^2 \cdot K)$		
V	Volume	m^3		
W	Air resistance	m/s		
X	Moisture ratio	kg/kg		
Z	Diffusion resistance	m/s		
α	Thermal expansion coefficient	K^{-1}		
α	Absorptivity	-		
β	Surface film coefficient for diffusion	s/m		
β	Volumetric thermal expansion coefficient	K^{-1}		
η	Dynamic viscosity	$N \cdot s/m^2$		
θ	Temperature	°C		
λ	Thermal conductivity	$W/(m \cdot K)$		
и	Vapour resistance factor	-		
ν	Kinematic viscosity	m^2/s		

4 0 Introduction

Symbol	Meaning	Units
$\overline{\rho}$	Density	kg/m ³
ρ	Reflectivity	-
σ	Surface tension	N/m
τ	Transmissivity	-
ϕ	Relative humidity	_
α, ϕ, Θ	Angle	rad
ξ	Specific moisture capacity	kg/kg per unit of moisture potential
Ψ	Porosity	-
Ψ	Volumetric moisture ratio	m^3/m^3
Φ	Heat flow	W

Table 0.2. List with suffixes and notations.

Symbol	Meaning			
Indices				
A	Air			
c	Capillary, convection			
e	Outside, outdoors			
h	Hygroscopic			
i	Inside, indoors			
cr	Critical			
CO ₂ , SO ₂	Chemical symbol for gases			
m	Moisture, maximal			
r	Radiant, radiation			
sat	Saturation			
s	Surface, area, suction			
rs	Resulting			
V	Water vapour			
W	Water			
ϕ	Relative humidity			
Notation				
[], bold	Matrix, array, value of a complex number			
Dash	Vector (ex.: \overline{a})			

0.3 References and literature

- [0.1] CIB-W40 (1975). Quantities, Symbols and Units for the description of heat and moisture transfer in Buildings: Conversion factors, IBBC-TNP, report No. BI-75-59/03.8.12, Rijswijk.
- [0.2] ISO-BIN (1985). Standards series X02-101 X023-113.
- [0.3] Kumaran, K. (1996). *Task 3: Material Properties*. Final Report IEA EXCO ECBCS Annex 24. ACCO, Louvain, p. 135.

1 Timber-framed construction

1.1 In general

In the Low Countries on the North Sea, timber was the common construction material for rural and municipal dwellings until the $13^{th}-14^{th}$ century. Brick construction was an aristocrat's privilege. Many devastating town fires, the sociological fact that bricks stood for wealth and growing wood shortages slowly turned brick building into the new standard.

Timber construction still is the reference in many countries worldwide, like the US, Canada, Norway, Sweden, Finland, Russia, Japan and other countries rich in forests and often with a cold climate. There, the framed type has an important advantage compared to massive construction: it is easy to insulate, which is why even in northwest Europe timber-frame construction has regained popularity, now for passive houses. However, the disadvantages also deserve mentioning: hardly any thermal inertia, air tightness critical and less moisture tolerant than brick construction.

In timber framing, load- and non-bearing outer and partitions walls consist of a framework of timber studs and crossbeams, called plates. The outer wall frames are externally finished with structural sheathing. Where the studs bear all vertical loads and the outer wall ones have also to withstand the wind component, normal to the façade, the sheathing provides overall stiffness against horizontal loading. It also prevents buckling of the studs parallel to their lowest inertia radius. From the three common framing approaches – platform, balloon, post and beam – the platform type, composed of storey-high stud walls and timber floors is the most popular (Figure 1.1).

Construction looks as follows: once the foundations and foundation walls are ready, the ground floor is laid, in humid climates preferably a concrete deck, though in dry climates also timber joists with plywood or OSB (oriented strand board) deck apply, the crosscut end sides being closed with header plates. In such case, ripped half-width standard timber beams form the floor joists with struts at half-span excluding lateral buckling. Then one fixes the bottom plates, after which the studs are nailed and coupled with top plates. To stabilize the frame corners, doubling these is an option. After, a plywood, OSB or stiff insulation board (XPS) sheathing is nailed to the outer wall frames. The joists of the second floor, which are fixed at the top plates then follow. Header plates again close the crosscut end sides and plywood or OSB forms the running surface. The same cycle restarts for the second storey: bottom plate, studs, top plates, sheathing, floor joists, running surface, etc.

A timber framework or rafters, axis to axis at the same distance as the studs, shape the load-bearing roof structure with an external sheathing once more providing stiffness. Timber framing ends with wrapping up the outer walls with waterproof, wind tight building paper, stapled from bottom to top on the sheathing with the higher strips overlapping the lower ones. Platform framing lends itself to modular construction and prefabrication.

From inside to outside the outer wall assembly looks like (Figure 1.2): inside lining (gypsum board); (service cavity); air (always) and vapour (when necessary) retarder; bays between studs filled with insulation (mineral wool or cellulose); plywood, OSB or stiff insulation board sheathing; building paper; outside finish (timber siding, brick veneer, EIFS, etc).

Aside from timber framing, also metal framed construction exists, with metal studs and plates replacing the timber ones.

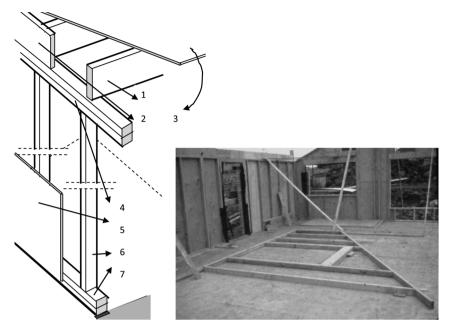


Figure 1.1. Platform type (1: joists, 2: header plate, 3: running surface, 4: top plates, 5: sheathing, 6: studs, 7: bottom plates).

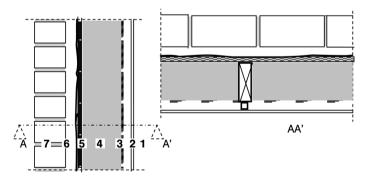


Figure 1.2. Timber-framed outer wall, reference assembly (1: inside lining, 2: service cavity, 3: air and vapour retarder, 4: thermal insulation; 5: sheathing, 6: building paper, 7: outside finish).

1.2 Performance evaluation

1.2.1 Structural integrity

Timber-framed buildings are so lightweight that anchoring in the foundation walls is necessary to prevent displacement under extreme wind load (Figure 1.3).

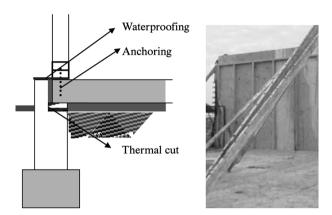


Figure 1.3. Timber-framed construction, anchoring in the foundation walls.

Wind loading and buckling of the outer and partition wall studs demands proper attention. The sheathing or inside finishes block it in the lowest moment of inertia direction. The direction normal to the walls needs a control. Table 1.1 gives the buckling factors vertical loads have to be multiplied by, as a function of the stud's slenderness (*i*):

$$i = \frac{L}{\sqrt{\frac{I}{A}}} \tag{1.1}$$

with L the effective stud span (in timber framed construction equal to the distance between bottom and top plates), I the moment of inertia around the neutral axis of the combination stud/sheathing (if shear-stiff coupled) and A total active cross section.

If this product gives stresses in the timber beyond acceptable, or, if for a given span the stud's radius of inertia is too low, then two options are left: diminishing the centre-to-centre distance between studs or using deeper ones. The first is disadvantageous in terms of whole wall thermal transmittance whereas the second allows larger insulation thicknesses, thus, a lower whole wall thermal transmittance.

Table 1.2 summarizes the mechanical properties of softwood and plywood. For the stiffness against horizontal loads, the same rules as for massive construction hold: the floors as rigid horizontal decks, at least 3 sheathed or wind-braced walls whose centre planes do not cross in one point, the stiff walls preferentially distributed in a way the resulting wind load vector crosses their stiffness centre.

Table 1.1. Buckling factors (slenderness vertically in steps of 10, horizontally in steps of 1).

Slenderness	0	1	2	3	4	5	6	7	8	9
0	1	1	1.01	1.01	1.02	1.02	1.02	1.03	1.03	1.04
10	1.04	1.04	1.05	1.05	1.06	1.06	1.06	1.07	1.07	1.08
20	1.08	1.09	1.09	1.10	1.11	1.11	1.12	1.13	1.13	1.14
30	1.15	1.16	1.17	1.18	1.19	1.20	1.21	1.22	1.24	1.25
40	1.26	1.27	1.29	1.30	1.32	1.33	1.35	1.36	1.38	1.40
50	1.42	1.44	1.46	1.48	1.50	1.52	1.54	1.56	1.58	1.60
60	1.62	1.64	1.67	1.69	1.72	1.74	1.77	1.80	1.82	1.85
70	1.88	1.91	1.94	1.97	2.00	2.03	2.06	2.10	2.13	2.16
80	2.20	2.23	2.27	2.31	2.35	2.38	2.42	2.46	2.50	2.54
90	2.58	2.62	2.66	2.70	2.74	2.78	2.82	2.87	2.91	2.95
100	3.00	3.06	3.12	3.18	3.24	3.31	3.37	3.44	3.50	3.57
110	3.63	3.70	3.76	3.83	3.90	3.97	4.04	4.11	4.18	4.25
120	4.32	4.39	4.46	4.54	4.61	4.68	4.76	4.84	4.92	4.99
130	5.07	5.15	5.23	5.31	5.39	5.47	5.55	5.63	5.71	5.80
140	5.88	5.96	6.05	6.13	6.22	6.31	6.39	6.48	6.57	6.66
150	6.75	6.84	6.93	7.02	7.11	7.21	7.30	7.39	7.49	7.58
160	7.68	7.78	7.87	7.97	8.07	8.17	8.27	8.37	8.47	8.57
170	8.67	8.77	8.88	8.98	9.08	9.19	9.29	9.40	9.61	9.61
180	9.72	9.83	9.94	10.05	10.16	10.27	10.38	10.49	10.60	10.72
190	10.83	10.94	11.06	11.17	11.29	11.41	11.52	11.64	11.76	11.88
200	12.00	12.12	12.24	12.36	12.48	12.61	12.73	12.85	12.98	13.10
210	13.23	13.36	13.48	13.61	13.74	13.87	14.00	14.13	14.26	14.39
220	14.52	14.65	14.79	14.92	15.05	15.19	15.32	15.46	15.60	15.73
230	15.87	16.01	16.15	16.29	16.43	16.57	16.71	16.85	16.99	17.14
240	17.28	17.42	17.57	17.71	17.86	18.01	18.15	18.30	18.45	18.60

Table 1.2. Mechanical properties of softwood and plywood.

Property		Softwood			Plywood		
			Class 1	Class 2	Class 3	// fibres outer laminates	+ fibres outer laminates
Modulus of e	lasticity	MPa					
∥ fibres ⊥ fibres		11 000 300			7 000 3 000		
Shear modulus MPa			500				
Allowed stres	ss						
Bending	// fibres ⊥ plywood // plywood	MPa MPa MPa	7	10	13	13 9	5 6
Tension	// fibres // plywood	MPa MPa	0	8.5	10.5	8	4
Compression	<pre>// fibres ⊥ fibres ⊥ plywood // plywood</pre>	MPa MPa MPa MPa	6 2	8.5	11 2	3 8	3 4
Shear	∥ fibres ⊥ plywood ∥ plywood	MPa MPa MPa	0.9	0.9	0.9	1.8 0.9	1.8 0.9

1.2.2 Building physics: heat, air, moisture

1.2.2.1 Air tightness

Air tightness of timber-framed envelopes is not taken for granted. The outside finish, the building paper, the sheathing, as well as the insulation, all are air-permeable. Contributing factors are, for the building paper, the overlaps between the strips, for the sheathing the joints between boards and for the thermal insulation the material itself and the gaps between insulation, studs and plates. It is the inside finish to guarantee air-tightness. Non-perforated gypsum board linings without cracks between boards have an air permeance of $(K_a) \approx 3.1 \cdot 10^{-5} \Delta P_a^{-0.19}$. For an air pressure difference of 10 Pa, that value limits air leakage to 0.43 m³/(m² · h). However, when sockets and others perforate the lining and cracks form between boards, this value may increase by a factor of 10, which is why inclusion of an additional air barrier deserves recommendation. In moderate and cold climates, one used a PE-foil, stapled against the timber frame, preferentially with a service cavity left between foil and inside lining. Recently, OSB with taped joints emerged as an alternative (Figure 1.4). But also with additional air barrier, perfect air-tightness is hard to realize. Even excellent workmanship did not result in tested air leakages below 3 dm³/(m² · h) at 1 Pa air pressure difference. In hot and humid climates, it is up to the outside finish to guarantee air-tightness.