



Adam Szymkiewicz

Modelling Water Flow in Unsaturated Porous Media

Accounting for Nonlinear Permeability
and Material Heterogeneity

 Springer

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Adam Szymkiewicz
Faculty of Civil and Environmental Engineering
Gdansk University of Technology
Gdansk
Poland

The GeoPlanet: Earth and Planetary Sciences Book Series is in part a continuation of Monographic Volumes of Publications of the Institute of Geophysics, Polish Academy of Sciences, the journal published since 1962 (<http://pub.igf.edu.pl/index.php>).

ISSN 2190-5193 ISSN 2190-5207 (electronic)
ISBN 978-3-642-23558-0 ISBN 978-3-642-23559-7 (eBook)
DOI 10.1007/978-3-642-23559-7
Springer Heidelberg New York Dordrecht London

Library of Congress Control Number: 2012945473

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Acknowledgments

I owe very special thanks to Prof. Rainer Helmig, Head of the Department of Hydromechanics and Modeling of Hydrosystems in the Institute for Modeling Hydraulic and Environmental Systems, University of Stuttgart, who invited me several times to work with his research group. His help and advice were essential for the preparation of the present book. During my stay in Stuttgart I was supported by the German Research Foundation (DFG), in the framework of the Cluster of Excellence in Simulation Technology (SimTech, EXC 310/1), as well as by the International Training Group *Non-linearities and Upscaling in Porous Media* (NUPUS). The aid received from these two institutions is kindly acknowledged here.

A significant part of this book is based on the research work which I carried out together with Prof. Jolanta Lewandowska and I very much appreciate our long lasting cooperation. I also greatly benefitted from the collaboration with Prof. Insa Neuweiler, Prof. Kazimierz Burzyński, Prof. Michel Vauclin, Prof. Jean-Louis Auriault, Prof. Rafael Angulo-Jaramillo, Prof. Sorin Pop, Dr. Joanna Butlańska, and Dr. Alexandru Tatomir.

I am much indebted to Prof. Paweł Rowiński, editor of the Springer Geoplanet series, for the possibility of publishing my manuscript. Moreover, I would like to acknowledge the support and encouragement received from Prof. Zbigniew Sikora, Head of the Department of Geotechnics, Geology and Marine Engineering at the Faculty of Civil and Environmental Engineering, Gdańsk University of Technology, Prof. Ireneusz Kreja, dean of the Faculty, Prof. Eugeniusz Dembicki, Prof. Henryk Zaradny, and Prof. Jarosław Napiórkowski. Thanks to all the colleagues from the Department of Geotechnics in Gdańsk and from the Department of Hydromechanics in Stuttgart for a friendly atmosphere, which helped me substantially in my work.

I am very grateful to Prof. Rainer Helmig, Prof. Insa Neuweiler, Prof. Zbigniew Sikora and my father, Prof. Romuald Szymkiewicz, for careful reading of the manuscript and many helpful suggestions. Any remaining errors are entirely my

own responsibility. I also greatly appreciate the help received from Ms. Agata Oelschlager, Ms. Anna Dziembowska, Mr. Gowrishankar Chakkravarthy and his team in the preparation of this book.

Last, but not least, many thanks are to my wife Maria, my daughter Lidia and my parents Iwona and Romuald, for their constant love and support.

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Notations

Subscripts related to fluid phases:

a	Air,
w	Water,
α	Generic fluid phase.

Subscripts related to the components of vectors and tensors (Einstein summation convention is implied only for these subscripts): i, j, k, l, m, n .

Superscripts related to spatial discretization (in parentheses)

(i) to (m)	Indices of grid entities: nodes, elements, volumes or faces,
(ij)	Average value between nodes i and j ,
(e)	Average value in a finite element,
(fc)	Average value at a finite volume face,
(τ)	Time step index,
(v)	Iteration index.

Superscripts related to components of a heterogeneous medium:

I	Fracture system or background material
II	Rock matrix or inclusions

Superscripts related to averaged field-scale properties:

eff	Effective parameter,
eq	Equivalent parameter.

Superscripts related to homogenization analysis:

*	Dimensionless variable,
(c)	Characteristic value.

Symbols (physical units specified where appropriate):

Uppercase Latin letters:

$A_{\alpha}^{(ij)}$	Coefficients in spatially discretized flow equations for phase α at node j ,
B_{ij}^{high}	Geometry-dependent constant for calculating the effective water permeability in a medium with highly permeable inclusions,
B_{ij}^{low}	Geometry-dependent constant for calculating the effective water permeability in a medium with weakly permeable inclusions,
$C_{\text{it}}^{\text{dec}}$	Coefficient decreasing the time step size,
$C_{\text{it}}^{\text{inc}}$	Coefficient increasing the time step size,
C_{ch}	Specific water capacity in the pressure head based form of the Richards equation, (m^{-1}),
C_{wh}	Storage coefficient in the pressure head based form of the Richards equation, (m^{-1}),
C_{wp}	Storage coefficient in the pressure based form of the Richards equation, (Pa^{-1}),
D	Hydraulic diffusivity tensor, ($\text{m}^2 \text{s}^{-1}$),
D_e	Energy dissipation for fluid flow in porous medium, (Pa^2),
D_L	Characteristic diffusivity at the field scale (m),
D_I	Characteristic diffusivity at the Darcy scale (m),
$E^{(n)}$	n th finite element,
$F^{(n)}$	n th face of a finite volume grid,
$G_{\alpha}^{(j)}$	Gravity term in spatially discretized flow equation for phase α at node j ,
H_{α}	Total potential head of fluid phase α , (m),
K_{sz}	Hydraulic conductivity of phase α at apparent saturation, (m s^{-1}),
K_{α}	Hydraulic conductivity of phase α , (m s^{-1}),
L	Characteristic length at the field scale, (m),
M_{α}	Mass density of fluid phase α with respect to the bulk volume of porous medium, $M_{\alpha} = \rho_{\alpha} \phi_{\alpha} S_{\alpha}$, (kg m^{-3}),
$Q_{\alpha}^{(\text{fc})}$	Total mass flux of phase α at a control volume face, (kg s^{-1}),
R_b	Characteristic dimension of a matrix block or inclusion, (m),
R_{gas}	Universal gas constant, ($\text{J}(\text{mol}^{\circ}\text{K})^{-1}$),
$S_{\text{a}}^{\text{trap}}$	Effective air saturation for a heterogeneous medium in trapped-air regime,
$S_{\text{w}}^{\text{trap}}$	Effective water saturation for a heterogeneous medium in trapped-air regime,
S_{α}	Saturation of fluid phase α ,
$S_{\text{e}\alpha}$	Normalized saturation of phase α ,
S_{α}^{max}	Maximum attainable saturation of phase α ,
S_{α}^{min}	Minimum attainable saturation of phase α ,

S_{rx}	Saturation of phase α at residual state,
T_x^m	Non-equilibrium mass flow rate between fractures and matrix, or between background material and inclusions, $(\text{kg}(\text{m}^3 \text{s})^{-1})$,
T_x^v	Non-equilibrium volumetric flow rate between fractures and matrix, or between background material and inclusions, (s^{-1}) ,
U	Domain of a representative elementary volume at the pore scale,
U_x	Part of a pore-scale representative elementary volume occupied by phase α ,
V_b	Matrix block domain,
$V^{(i)}$	i th finite volume,
W	Solution domain at the Darcy scale,
Z_k	Auxiliary parameter in the formula for inter-nodal permeability,
Z_s	Auxiliary parameter in the formula for relating parameters of the Brook-Corey and van Genuchten functions.

Calligraphic Latin letters:

$\mathcal{D}^{(j)}$	Spatial discretization operator for node j ,
$\mathcal{E}^{(j)}$	Set of finite elements sharing node j ,
\mathcal{H}	Relative air humidity,
\mathcal{M}_α	Mole mass of fluid phase α , (kg mol^{-1}) ,
$\mathcal{N}_{\text{elem}}^{(n)}$	Set of nodes belonging to n -th finite element,
$\mathcal{N}_{\text{nod}}^{(j)}$	Set of nodes connected to node j , including j ,
$\mathcal{O}(u)$	Order of magnitude of number u ,
\mathcal{R}_c	Dimensionless gravity–capillarity ratio,
\mathcal{R}_d	Dimensionless hydraulic diffusivity ratio between inclusions and background,
\mathcal{R}_k	Dimensionless permeability ratio between inclusions and background,
\mathcal{R}_t^l	Dimensionless time scale for Darcy-scale flow in porous material l ,
\mathcal{T}	Kelvin temperature, $(^\circ\text{K})$.

Lowercase Latin letters:

a_i	Length of the ellipsoidal inclusion in i th spatial direction, (m),
$a', a'_{10}, a'_{11}, a'_2$	Parameters in the Gasto et al. formula for the inter-nodal permeability,
$b', b'_{01}, b'_{02}, b'_1$	Parameters in the Gasto et al. formula for the inter-nodal permeability,
c', c'_0	Parameters in the Gasto et al. formula for the inter-nodal permeability,
d_i	Ellipsoid depolarisation coefficient in i th spatial direction,
f_z	Fractional flow function for fluid phase α ,
g	Magnitude of the gravitational acceleration vector, (m s^{-2}) ,

\mathbf{g}	Gravitational acceleration vector, (m s^{-2}),
h_α	Pressure head of fluid phase α , (Pa),
h_c	Capillary pressure head, (Pa),
h_e	Air-entry pressure head, (Pa),
h_g	Pressure head scaling parameter, (Pa),
$k_{ca}^{(ij)}$	Average relative water permeability for the capillary-driven flow between nodes i and j ,
$k_{gr}^{(ij)}$	Average relative water permeability for the gravity-driven flow between nodes i and j ,
$k_{int}^{(ij)}$	Integrated average relative water permeability between nodes i and j ,
k_{ii}^{cpl}	Cardwell and Parsons lower bound for the equivalent permeability in i th direction, $i = 1, 2, 3$, (m^2),
k_{ii}^{cpu}	Cardwell and Parsons upper bound for the equivalent permeability in i th direction, $i = 1, 2, 3$, (m^2),
$k_{rw}^{(el)}$	Average relative water permeability in a finite element,
k_{rw}^{fm}	Relative water permeability at the fracture–matrix interface,
$k_{rw}^{(ij)}$	Average relative water permeability between nodes i and j ,
$k_{r\alpha}$	Relative permeability of phase α ,
\mathbf{K}_s	Intrinsic permeability tensor, (m^2),
\mathbf{K}_s^{eq}	Equivalent intrinsic permeability tensor of heterogeneous medium, (m^2),
\mathbf{K}_s^{eff}	Effective intrinsic permeability tensor of a heterogeneous medium, (m^2),
\mathbf{k}_t	Total permeability tensor in fractional flow formulation, ($\text{m}^2(\text{Pa s})^{-1}$),
\mathbf{k}_α	Permeability tensor of phase α , (m^2),
\mathbf{K}_α^{eff}	Effective permeability tensor of a heterogeneous medium for phase α , (m^2),
\mathbf{K}_w^{high}	Effective water permeability tensor for a heterogeneous medium with highly permeable inclusions, (m^2),
\mathbf{K}_w^{low}	Effective water permeability tensor for a heterogeneous medium with weakly permeable inclusions, (m^2),
\mathbf{K}_w^{trap}	Effective water permeability tensor for a heterogeneous medium in trapped-air regime, (m^2),
l	Characteristic length at the Darcy scale, (m),
l_h	Characteristic dimension of Darcy-scale heterogeneities, (m),
l_v	Characteristic dimension of the averaging volume, (m),
m_g	Exponent in the van Genuchten capillary function,
n_b	Exponent in the Brooks–Corey capillary function,
n_g	Exponent in the van Genuchten capillary function,

\mathbf{n}_E	Unit vector normal to the boundary of a finite element,
\mathbf{n}_V	Unit vector normal to the boundary of a finite volume,
\mathbf{n}_W	Unit vector normal to the boundary of the porous domain,
\mathbf{n}	Unit vector normal to the interface separating two porous materials,
p_{atm}	Atmospheric pressure, (Pa),
p_c	Capillary pressure, (Pa),
p_e	Air-entry pressure, (Pa),
p_e^{drain}	Air-entry pressure during drainage, (Pa),
p_e^{wet}	Air-entry pressure during wetting, (Pa),
p_g	Capillary pressure scaling parameter in the Gardner and van Genuchten functions, (Pa),
p_α	Pressure in fluid phase α , (Pa),
p_α^{ref}	Reference pressure for fluid phase α , (Pa),
p_{glob}	Global pressure in the fractional flow formulation, (Pa),
\tilde{p}_i	Fluctuation of the fluid pressure for steady flow in i th spatial direction, (Pa),
q_{ev}	Cumulative evaporation flux at the soil surface, (m),
q_{inf}	Cumulative infiltration flux at the soil surface, (m),
r_b	Local spatial coordinate in a matrix block or inclusion, (m),
r_c	Radius of a capillary tube, (m),
r_{c1}, r_{c2}	Main curvature radii of the air–water interface, (m),
s_{abs}	Absolute error tolerance in the solution of nonlinear algebraic equations,
s_{rel}	Relative error tolerance in the solution of nonlinear algebraic equations,
t	Time, (s),
t_{dry}	Surface drying time in the evaporation simulation, (s),
t_{pond}	Surface ponding time in the infiltration simulation, (s),
u	Generic variable,
\mathbf{u}	Vector of unknown nodal values in the numerical solution,
v_L	Characteristic advective velocity at the field scale, (m s^{-1}),
v_l	Characteristic advective velocity at the Darcy scale, (m s^{-1}),
$v_{\text{st}}^{(ij)}$	Steady-state volumetric water flux between nodes i and j , (m s^{-1}),
v_w^{top}	Volumetric water flux at the soil surface, (m s^{-1}),
\mathbf{v}_α	Volumetric flux of fluid phase α with respect to the solid phase (Darcy velocity), (m s^{-1}),
\mathbf{v}_t	Total volumetric flux in the fractional flow formulation, (m s^{-1}),
w	Volumetric fraction of a porous material,
\mathbf{x}	Spatial coordinate vector, (m),
\mathbf{y}	Spatial coordinate vector associated with a periodic cell, (m),
z	Elevation above the reference level, (m).

Uppercase Greek letters:

Γ	Interface between two porous materials,
$\Delta x^{(ij)}$	Distance between nodes i and j , (m),
$\Delta x'$	Normalized distance between nodes,
Δt	Time step, (s),
Θ	Weighting coefficient in the time discretization scheme,
Λ^b	External surface of a matrix block,
$\Lambda^{(i+1/2)}$	Interface between nested matrix blocks i and $i + 1$ in MINC method,
Υ	Weighting function in the finite element method,
Φ_h	Flux potential with respect to the water pressure head, (m),
Φ_p	Flux potential with respect to the water pressure, (Pa),
$\Psi^{(i)}$	Shape function for node i in the finite element method,
$\Psi_e^{(i)}$	Element shape function for node i in the finite element method,
Ω	Domain of a periodic cell,
Ω'	Part of a periodic cell occupied by the background material,
Ω''	Part of a periodic cell occupied by the inclusions.

Lowercase Greek letters:

α_g	Inverse of the scaling pressure (or pressure head) in the capillary function, (Pa^{-1}) or (m^{-1}),
$\alpha_{p,q}$	Coefficients in the modified equation,
β_α	Relative compressibility coefficient for fluid phase α , (Pa^{-1}),
β^{fm}	Shape coefficient for the fracture–matrix transfer term,
β'	Parameter in the averaging formula for the inter-nodal permeability,
$\beta_{p,q}$	Coefficients in the modified equation,
γ^{fm}	Scaling coefficient for the fracture–matrix transfer term,
$\gamma_{p,q}$	Coefficients in the modified equation,
$\delta \mathbf{u}$	Increment of the vector of unknown values in the iterative solution procedure,
ε	Scale parameter,
ζ	Gravity coefficient, cosine of the angle between x axis and the gravity vector in one-dimensional problems,
ζ'	Modified gravity coefficient,
η_α	Exponent in the power-law relative permeability function for phase α ,
$\eta_1, \eta_2, \eta_3, \eta_4$	Exponents in the Mualem and Burdine relative permeability functions,
θ_α	Volumetric content of phase α ,

θ_{rx}	Volumetric content of phase at the residual state α ,
θ_{sz}	Volumetric content of phase α at the state of apparent saturation,
θ_a^{trap}	Effective volumetric air content for a heterogeneous medium in trapped-air regime,
θ_w^{trap}	Effective volumetric water content for a heterogeneous medium in trapped-air regime,
κ	Connectivity parameter in the Mualem and Burdine relative permeability functions,
λ_α	Mobility of phase α , $(\text{Pa s})^{-1}$,
μ_α	Dynamic viscosity coefficient of fluid phase α , (Pa s) ,
ξ	Local spatial coordinate in the finite element scheme,
π_i	Weighting coefficient in the generalized power average formula for the equivalent permeability in i th spatial direction,
ρ_α	Intrinsic mass density of fluid phase α , (kg m^{-3}) ,
ρ_α^{ref}	Reference intrinsic mass density of fluid phase α , (kg m^{-3}) ,
$\sigma_{\alpha\beta}$	Surface tension between phases α and β , (N m^{-1}) ,
ν	Small number used in numerical differentiation,
ϕ	Porosity,
χ_i	Auxiliary variable used to define the effective permeability in i th spatial direction,
	Wetting angle,
ω_k	Weighting parameter in the averaging scheme for fracture–matrix permeability,
ω_v	Weighting parameter in the averaging formula for the inter-nodal relative permeability,
ω_w	Weighting parameter in the averaging formula for the inter-nodal relative permeability.

Chapter 1

Introduction

The unsaturated zone, also called vadose zone, is located between the soil surface and the groundwater table. Its depth is variable and depends on geological and climatic factors. As the name implies, soils and rocks in the unsaturated zone are only partially filled with water, the rest of the pore space being occupied by air. The vadose region constitutes a vital link between groundwater, atmospheric water and surface water. It is a place of intense human activity of various kinds, including civil and environmental engineering and agriculture. Therefore, flow and transport phenomena occurring in the unsaturated zone can be studied from different viewpoints, as shown schematically in Fig. 1.1.

A distinct scientific specialization, soil physics, is entirely devoted to the study of physical processes in soils, including the water flow in unsaturated conditions, e.g. [17, 20, 47]. Soil physics developed in a close relationship to agronomy and hydrology. In agricultural applications, emphasis is put on the availability of water and dissolved nutrition substances to plants, which motivates the development of comprehensive models to describe the soil-plant-atmosphere system, e.g. [8, 9]. Accurate evaluation of water infiltration into the soil and evapotranspiration from the soil is also important for hydrological models. For instance, the infiltration capacity of soils has a direct influence on the formation of runoff, and thus is an important factor in predicting the risk of flood. Consequently, a trend towards explicit coupling of the surface and shallow subsurface flow in hydrological models can be observed, e.g. [11, 48].

On the other hand, the water flow processes in the unsaturated zone have significant impact on groundwater flow in saturated aquifers, which constitute a major source of drinking water. Even more importantly, the vadose zone is a buffer between groundwater and various sources of pollutants located at the soil surface or in the shallow subsurface. Reliable prediction of the fate of contaminants dissolved in water requires the knowledge of water flow velocities in the unsaturated zone, which are in general highly variable in space and time. Therefore, increasing attention is paid to coupled saturated-unsaturated models of groundwater flow and contaminant transport, e.g. [43, 44, 50]. Moreover, accounting for the unsaturated flow allows for

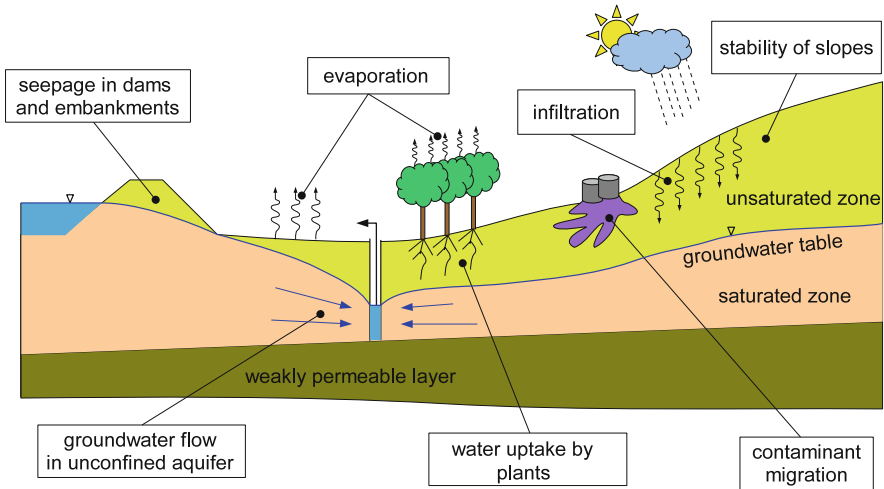


Fig. 1.1 Typical problems related to water flow in the vadose zone

improved estimation of parameters related to the hydraulics of phreatic aquifers, such as the recharge rate [18], the specific yield [35] or the height of the seepage face in wells [5].

Water flow in the vadose zone has important implications also for geotechnical engineering. Traditionally, soil mechanics focused mostly on completely dry or fully saturated non-cohesive soils, and fully saturated cohesive soils. However, a wide range of problems can be more accurately modelled, if the variability in the soil water saturation is taken into account. This is particularly necessary for soils that swell, shrink or collapse due to the changes in water saturation, but there is an increasing awareness of the importance of unsaturated flow also for other applications, including soil compaction, slope stability, flow in dams and embankments, protection of landfills, tunneling or interpretation of penetration tests, e.g. [30, 31, 51]. Unsaturated soil mechanics is still an emerging and very active field of research, which developed substantially during the last twenty years, e.g. [10, 25, 28].

In all the applications mentioned above a crucial issue is the ability to accurately model water flow in soils, or—more generally—partially saturated porous media. This, however, is a challenging task, due to the multi-phase and multi-scale nature of porous media, especially the ones formed by natural processes. Porous soils and rocks in the vadose zone consist of several deformable solid and fluid phases, separated by clearly distinguishable interfaces, representing sharp discontinuities in physical and chemical properties [16, 33]. In general, each of the phases consists of multiple chemical components, which can move between phases. Pore air, for instance, is a mixture of gases, including water vapor, while pore water contains many dissolved substances, including gases. The number of phases and components included in the mathematical model depends on the problem under consideration. In many applications focusing on the water flow, a sufficient accuracy can be achieved with

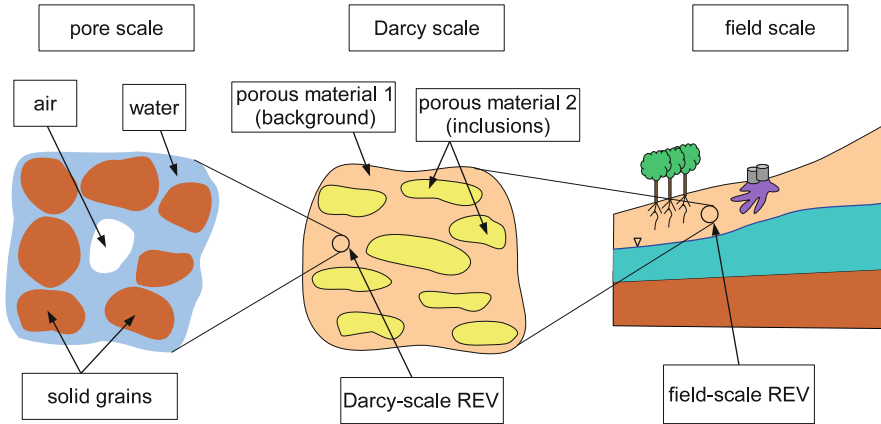


Fig. 1.2 Observation scales in a porous medium

a simplified model, where both air and water are considered as immiscible single-component phases and the deformation of the solid skeleton is neglected. Such an approach is adopted in the present work.

Modelling of flow in porous media is further complicated by the fact that the relevant physical processes can be described at various observation scales. Mathematical models applied at each scale typically represent the principles of conservation of basic quantities such as mass, momentum and energy, but the exact form of the governing equations may differ substantially between the scales. In some cases the model describing processes at a larger scale can be derived directly from the equations relevant at a smaller scale by an appropriate averaging procedure. This process is known as upscaling. Alternatively, the governing equations can be formulated directly at the larger scale, based on phenomenological considerations. Two basic scales, typically distinguished in porous media, are the pore scale and the Darcy scale, Fig. 1.2. In the former case, the characteristic spatial dimension is the size of a single pore, which in granular media is approximately proportional to the grain size. At this scale, each phase occupies a distinct spatial domain, and each point of space can be associated with a specific phase. On the other hand, it is assumed that each phase can be regarded as a continuum within its own spatial sub-domain, i.e. the size of the pores is much larger than the size of fluid molecules. The flow of fluid phases can be described by the Navier-Stokes equations with appropriate conditions at the fluid-solid and fluid-fluid interfaces. However, the pore scale description is not suitable for practical problems, which involve spatial domains having dimensions larger than the pore size by many orders of magnitude. Therefore, the governing equations describing behaviour of various phases are usually formulated at a much larger scale, which in the present work will be referred to as the Darcy scale, from the name of H. Darcy, who developed the well-known formula for the water seepage velocity in a porous medium [7]. At this scale, each spatial point corresponds to a representative elementary volume (REV), containing a sufficiently large number of pores, occupied

by multiple fluid phases. Thus, in contrast to the pore scale description, at the Darcy scale each phase forms a continuum over the entire spatial domain.

The most commonly used two-phase model of air and water flow at the Darcy scale is a combination of the mass conservation equation for each fluid with the semi-empirical equation for flow velocity, based on an extension of the Darcy formula for the case of multi-phase flow. One of key components of the model is the capillary function, describing the relationship between the water saturation and the capillary pressure, defined as the difference between pressures in the air and water phases. A complementary constitutive relationship is given by the relative permeability function, which describes the ability of each fluid phase to flow in the porous medium as a function of the phase saturation. Both functions are strongly nonlinear. Their form depends principally on the geometrical characteristic of the pore space and on the properties of the fluid-fluid and fluid-solid interfaces (surface tension). The mathematical model of two-phase flow is often formulated as two coupled partial differential equations of parabolic type, with the two phase pressures or saturations as the primary unknown variables.

The two-phase model can be simplified, if one assumes that the air phase is continuously distributed in pores, it is connected to the atmospheric air and much more mobile than the water phase. Accordingly, the pressure in the air phase can be considered constant and equal to the atmospheric pressure, and the equation describing air flow is eliminated. The remaining equation for the water flow is called the unsaturated flow equation or the Richards equation [34]. Similarly to the full two-phase flow model, the Richards equation is based on semi-empirical concepts of the capillary and relative permeability functions, introduced at the Darcy scale to account for a number of pore scale phenomena, which at present are not fully understood. These constitutive relationships are difficult to associate with the Darcy-scale processes in a manner that is both physically rigorous and easy to implement practically. While a number of improved formulations for the two-phase and unsaturated flow have been proposed, e.g. [3, 14, 26, 29, 32, 49], the Richards equation remains a useful and well-established tool in the unsaturated zone modelling, and is the basis of the present analysis.

The present book focuses on two aspects of the application of the Richards equation. The first one is related to its numerical solution. Although significant development of the numerical algorithms occurred in the last twenty years, e.g. [4, 27], solution of the Richards equation remains a challenging task due to the afore-mentioned strongly nonlinear constitutive relationships, which must be appropriately represented in the discretized space-time domain. A particularly important issue is the approximation of the relative permeability between the nodes of a spatial grid, which is a necessary to estimate water fluxes, according to a discrete version of the Darcy formula. As the relative permeabilities may differ by several orders of magnitude (for example, during infiltration in a dry soil, or evaporation), the choice of the averaging method is often essential for the overall accuracy of the approximate solution. Several simple averaging schemes have been proposed, e.g. arithmetic mean, geometric mean and upstream weighting, but each of them may lead to large errors for particular combinations of the initial and boundary conditions, grid size and the form of

functional relationship between the relative permeability and the capillary pressure, e.g. [1, 2, 15]. On the other hand, more accurate methods often require significantly larger computational effort, e.g. [46]. In this work an averaging scheme is presented, that is relatively easy to implement and significantly improves the solution accuracy for a wide range of one- and two-dimensional problems. The method was proposed in the paper [36], and further developed in [37, 38]. Extension of the method for unstructured grids and implications for the solution of the full two-phase model are also discussed. The analysis is carried out for a simple form of the Richards equation, which does not account for soil compressibility nor water uptake by plant roots. While these two factors are very important in many applications related to the unsaturated zone and must be properly treated numerically, they have no direct influence on the development of the averaging schemes for inter-nodal permeabilities.

The second topic considered in this book deals with flow in porous media showing material heterogeneity at the Darcy scale. Heterogeneity may be related to various physical and chemical properties of the porous medium. The focus of this work is on porous formations composed of sub-domains characterized by distinct textural properties, which imply differences in pore geometry, and consequently in the physical parameters such as permeability, hydraulic diffusivity or air entry pressure (defined as the value of the capillary pressure above which the pore air flow is possible). The important issue of chemical heterogeneity, for instance related to the wettability and adsorption properties of the solid phase is not considered here. If the number of heterogeneous regions in the considered spatial domain is large, their explicit representation on a numerical grid becomes difficult or even impossible. Therefore, a new observation scale can be introduced, which for the purposes of this work will be called the field scale, Fig. 1.2. At this scale the relevant representative elementary volume encompasses sufficiently large number of Darcy scale heterogeneities to allow for the development of an upscaled model. The heterogeneous structure can be described in either deterministic or stochastic terms. In particular the stochastic models for flow and transport in unsaturated heterogeneous porous media have been a subject of intense research, e.g. [6, 12, 52]. In this book the deterministic viewpoint is adopted and a specific heterogeneity pattern is considered: a binary porous medium with disconnected porous inclusions (lenses) embedded in a continuous porous background material. While such a structure is relatively simple, it is representative of a number of natural porous formations, such as fluvial or coastal sediments, or sandstone-shale sequences, e.g. [19]. On the other hand, this type of pattern can be conveniently parametrized and analysed from the theoretical point of view, allowing for a good general understanding of local heterogeneities on the large-scale behaviour of the medium. The second part of this work presents an extended discussion of several models based on the Richards equation, which were developed for such type of media using the asymptotic homogenization approach [21–24, 39, 41]. These works showed that the macroscopic behaviour of the medium depends on the ratio between the permeabilities of the inclusions and the background material. A generalized model, valid for a wide range of inclusion-to-background permeability ratio, was proposed [39], and its preliminary experimental verification was carried out [40]. It can be also shown that the Richards approximation is not valid for media

characterized by higher value of the air-entry pressure in the matrix than in inclusions. In porous media showing heterogeneity with respect to the air-entry pressure the assumption of the continuity of air phase in porous medium, which underlies the Richards equation, may not be satisfied [41]. However, the accuracy of the Richards equation can be improved, if the large-scale capillary and permeability functions are appropriately modified [42].

The field scale discussed in this book represents an intermediate level in the hierarchy of scales relevant to the modeling of water flow in the vadose zone, with the characteristic length of the order of meters to dekameters. Significant research has been devoted to the description of unsaturated zone processes at regional scale, corresponding to hydrological watersheds, with the horizontal dimensions of many kilometers, e.g. [13, 45]. At such a scale, simplified mathematical models of the black-box type are routinely used and an important question is how to relate their parameters to the more detailed characteristics of the porous media available at smaller scales. While regional-scale hydrological modelling is of high practical importance, it is not considered in this book.

The book is structured as follows. Chapter 2 presents the mathematical formulation of flow in unsaturated porous medium. The governing equations for the two-phase model and the Richards model are discussed, together with various analytical formulae for capillary and permeability functions. In Chap. 3 a numerical algorithm to solve the governing flow equations is developed. The algorithm is formulated in general terms and can be applied to both the two-phase model and the Richards equation. Various methods of spatial discretization are discussed, including the control volume–finite difference and control volume–finite element approaches. The approximation of the average permeability in spatially discretized Richards equation is considered in detail in Chap. 4. Chapter 5 introduces basic concepts of upscaling. In Chap. 6 the upscaled models developed for flow in binary media without air-entry pressure effects are presented. The model accounting for air-entry effects is discussed in Chap. 7. The final chapter summarizes the contents of the book and outlines some open problems related to the discussed topics.

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