

Design of Power Management Integrated Circuits

Bernhard Wicht





Design of Power Management Integrated Circuits

Design of Power Management Integrated Circuits

Bernhard Wicht Leibniz University Hannover, Germany





This edition first published 2024 © 2024 John Wiley & Sons Ltd.

All rights reserved. No part of this publication may be reproduced, stored in a retrieval system, or transmitted, in any form or by any means, electronic, mechanical, photocopying, recording or otherwise, except as permitted by law. Advice on how to obtain permission to reuse material from this title is available at http://www.wiley.com/go/permissions.

The right of Bernhard Wicht to be identified as the author of the editorial material in this work has been asserted in accordance with law.

Registered Offices

John Wiley & Sons, Inc., 111 River Street, Hoboken, NJ 07030, USA John Wiley & Sons Ltd, The Atrium, Southern Gate, Chichester, West Sussex, PO19 8SQ, UK

For details of our global editorial offices, customer services, and more information about Wiley products visit us at www.wiley.com.

Wiley also publishes its books in a variety of electronic formats and by print-on-demand. Some content that appears in standard print versions of this book may not be available in other formats.

Trademarks: Wiley and the Wiley logo are trademarks or registered trademarks of John Wiley & Sons, Inc. and/or its affiliates in the United States and other countries and may not be used without written permission. All other trademarks are the property of their respective owners. John Wiley & Sons, Inc. is not associated with any product or vendor mentioned in this book.

Limit of Liability/Disclaimer of Warranty

While the publisher and authors have used their best efforts in preparing this work, they make no representations or warranties with respect to the accuracy or completeness of the contents of this work and specifically disclaim all warranties, including without limitation any implied warranties of merchantability or fitness for a particular purpose. No warranty may be created or extended by sales representatives, written sales materials or promotional statements for this work. This work is sold with the understanding that the publisher is not engaged in rendering professional services. The advice and strategies contained herein may not be suitable for your situation. You should consult with a specialist where appropriate. The fact that an organization, website, or product is referred to in this work as a citation and/or potential source of further information does not mean that the publisher and authors endorse the information or services the organization, website, or product may provide or recommendations it may make. Further, readers should be aware that websites listed in this work may have changed or disappeared between when this work was written and when it is read. Neither the publisher nor authors shall be liable for any loss of profit or any other commercial damages, including but not limited to special, incidental, consequential, or other damages.

Library of Congress Cataloging-in-Publication Data applied for:

Hardback ISBN: 9781119123064

Cover Design: Wiley Cover Image: © fotograzia/Getty Images

Set in 9.5/12.5pt STIXTwoText by Straive, Chennai, India

To my beloved family, Sabine, Luise, Friederike, Konstantin, and to my parents Siegrid and Eberhard.

Contents

Preface xvii

1 Introduction 1

- 1.1 What Is a Power Management IC and What Are the Key Requirements? 1
- 1.2 The Smartphone as a Typical Example 3
- 1.3 Fundamental Concepts 4
- 1.3.1 Using a Resistor The Linear Regulator 4
- 1.3.2 Using Switches and an Inductor The Inductive DC–DC Converter 4
- 1.3.3 Switches and Capacitors The SC Converter 6
- 1.3.4 Switches and Capacitors and Inductors The Hybrid Converter 6
- 1.4 Power Management Systems 7
- 1.5 Applications 8
- 1.5.1 IoT Nodes and Energy Harvesting 8
- 1.5.2 Portable Devices, Smartphones, and Wearables 9
- 1.5.3 Universal Serial Bus (USB) 11
- 1.5.4 Drones 11
- 1.5.5 Telecommunication Infrastructure 11
- 1.5.6 E-Bikes 12
- 1.5.7 Automotive 13
- 1.5.8 Data Centers 15
- 1.6 IC Supply Voltages 16
- 1.7 Power Delivery 17
- 1.7.1 Lateral and Vertical Power Delivery 18
- 1.7.2 Integrated Voltage Regulator (IVR) 19
- 1.7.3 Dynamic Voltage and Frequency Scaling (DVFS) 20
- 1.7.4 Near-Threshold Computing 22
- 1.8 Technology, Components, and Co-integration 22
- 1.8.1 Semiconductor Technology 22
- 1.8.2 Discrete Power Transistors 23
- 1.8.3 Passive Components 24
- 1.8.4 Co-integration 26
- 1.9 A Look at the Market 27 References 28

viii Contents

1	
2	The Power Stage 31
2.1	Introduction 31
2.2	On-Resistance and Dropout 32
2.3	Parasitic Capacitances 34
2.4	The Body Diode 35
2.5	Switching Behavior 37
2.5.1	Resistive Load 37
2.5.2	Inductive Load 39
2.5.3	Reverse Recovery and Switching Node Capacitance 41
2.5.4	Power and Gate Loop Inductance 42
2.5.5	Half-Bridge with Inductive Load 44
2.5.6	Switching Trajectories 45
2.6	Gate Current and Gate Charge 46
2.7	Losses 49
2.7.1	Conduction Losses 49
2.7.2	Conduction Losses in Case of Current Ripple 49
2.7.3	Dynamic Losses 51
2.7.4	Supply Current Related Losses 52
2.7.5	Total Losses 52
2.7.6	Switch Sizing for Minimum Losses 53
2.7.7	Losses in a Half-Bridge 55
2.8	Dead Time Generation 57
2.8.1	Fixed Dead Time 57
2.8.2	Adaptive Dead Time 58
2.8.3	Predictive Dead Time 58
2.9	Soft-Switching 59
2.9.1	Resonant Operation 60
2.9.2	Dead Time Control 60
2.10	Switch Stacking 61
2.11	Back-to-Back Configuration 63
	References 63
3	Semiconductor Devices 65
3.1	Discrete Power Transistors 65
3.1.1	The Silicon Power MOSFET 67
3.1.2	The Superjunction MOSFET 68
3.1.3	The Insulated-Gate Bipolar Transistor (IGBT) 68
3.1.4	The Gallium-Nitride Transistor 70
3.1.5	The Silicon-Carbide Transistor 71
3.2	Power Transistors in Integrated Circuits 72
3.2.1	Drain-Extended Transistors 72
3.2.2	Lateral DMOS Transistors 72
3.2.3	Silicon-on-Insulator Technologies (SOI) 77
3.2.4	Monolithic GaN Integration 78
3.3	Parasitic Effects 78
3.3.1	Parasitic Bipolar Junction Transistor 78
3.3.2	Capacitive Coupling 82

- 3.4 Safe Operating Area (SOA) 83
- 3.5 Integrated Diodes 85
- 3.5.1 Diodes with a Parasitic PNP Transistor 85
- 3.5.2 Diodes with a Parasitic NPN Transistor 86
- 3.5.3 The DMOS Transistor As a Power Diode 86
- 3.5.4 Zener Diodes 87 References 88

4 Integrated Passives 89

- 4.1 Capacitors 89
- 4.1.1 Metal-Oxide-Semiconductor Capacitors 89
- 4.1.2 Metal-Oxide-Metal Capacitors 91
- 4.1.3 Metal-Insulator-Metal Capacitors 91
- 4.1.4 Trench and Ferroelectric Capacitors 92
- 4.2 Inductors 93
- 4.2.1 Ampere's Law and Inductance 93
- 4.2.2 Bond-Wire and Package-Layer Inductors 94
- 4.2.3 Planar Metal-Layer Inductors 97
- 4.2.4 Inductors with Magnetic Core 103 References 104

5 Gate Drivers and Level Shifters 107

- 5.1 Introduction 107
- 5.2 Gate Driver Configurations 108
- 5.3 Driver Circuits 110
- 5.4 DC Characteristics 111
- 5.5 Driving Strength 113
- 5.6 The CMOS Inverter as a Gate Driver 114
- 5.6.1 Input and Output Capacitance 115
- 5.6.2 Output Current 115
- 5.6.3 Rise-Fall Time 116
- 5.6.4 Average Propagation Delay 117
- 5.6.5 Power Dissipation 117
- 5.7 Gate Driver with a Single-Stage Inverter *120*
- 5.7.1 Speed 120
- 5.7.2 Loss Energy *123*
- 5.8 Cascaded Gate Drivers 126
- 5.8.1 Optimization for Speed 128
- 5.8.2 Optimization for Energy Efficiency 130
- 5.9 External Gate Resistor 136
- 5.10 dv/dt Triggered Turn-On 137
- 5.10.1 Integrated Power Stages 138
- 5.10.2 Discrete Power Stages 139
- 5.10.3 Save Start-Up 140
- 5.11 Bootstrap Gate Supply 140
- 5.11.1 General Operation 140
- 5.11.2 Charge Balance and Bootstrap Capacitor Sizing 141

x Contents

- 5.11.3 Practical Aspects of Bootstrapping 142
- 5.11.4 Active Bootstrapping 143
- 5.12 Level Shifters 143
- 5.12.1 Resistor-Based Level Shifters 143
- 5.12.2 Cross-Coupled Level Shifters 147
- 5.12.3 Capacitive Level Shifters 151
- 5.12.4 Level-Down Shifters and Ground Level Shifters 155
- 5.13 Common-Mode Transient Immunity 156 References 159
- 6 **Protection and Sensing** 161
- 6.1 Overvoltage Protection 161
- 6.1.1 High-Voltage Cascode 161
- 6.1.2 Active Zener Diode 162
- 6.2 Overvoltage Protection for Inductive Loads 162
- 6.3 Temperature Sensing and Thermal Protection 165
- 6.4 Bandgap Voltage and Current Reference 167
- 6.4.1 Start-Up Circuit 169
- 6.4.2 Reference Current Generation 169
- 6.4.3 Accuracy 170
- 6.4.4 Trimming *170*
- 6.5 Short Circuits and Open Load 171
- 6.6 Current Sensing 173
- 6.6.1 Introduction 173
- 6.6.2 Replica Sensing 174
- 6.6.3 Shunt Current Sensing 178
- 6.6.4 DCR Sensing 181
- 6.6.5 Current Limit 183
- 6.7 Zero-Crossing Detection 187
- 6.8 Under-Voltage Lockout 189
- 6.9 Power-on Reset 190

References 193

7 Linear Voltage Regulators 195

- 7.1 Fundamental Circuit and Control Concept 195
- 7.2 Dropout Voltage 198
- 7.3 DC Parameters *199*
- 7.3.1 Power Efficiency 199
- 7.3.2 Current Efficiency 200
- 7.3.3 Load Regulation 201
- 7.3.4 Line Regulation 201
- 7.4 The Error Amplifier 203
- 7.5 Frequency Behavior and Stability 205
- 7.5.1 PMOS Type 205
- 7.5.2 NMOS Type 209
- 7.6 Transient Behavior 210
- 7.6.1 Voltage Under- and Over-Shoot 210

- 7.6.2 Fast Transient Techniques 213
- 7.6.3 Slew Rate Enhancement 213
- 7.6.4 Loop Bandwidth 214
- 7.7 Noise in Linear Regulators 214
- 7.8 Power Supply Rejection *216*
- 7.9 Soft-Start 217
- 7.10 Capacitor-Less LDO 218
- 7.11 Flipped Voltage Follower LDO 220
- 7.12The Shunt Regulator222
- 7.13 Digital LDOs 223
- 7.13.1 The Transistor Array 224
- 7.13.2 The Analog-to-Digital Converter 225
- 7.13.3 The Digital Controller 225
- 7.13.4 Transient Response 225
- 7.13.5 Power Supply Rejection 226
- 7.13.6 Limit Cycle Oscillations 227
- 7.13.7 Summary 227 References 227

8 Charge Pumps 229

- 8.1 Introduction 229
- 8.1.1 Fundamental Circuit and Operation 229
- 8.1.2 Charge Pumps Applications 230
- 8.1.3 General Characteristics 230
- 8.2 Analysis of the Fundamental Charge Pump 231
- 8.2.1 Step-Wise Ramp-Up 231
- 8.2.2 Voltage Droop for Nonzero Load 232
- 8.2.3 Output Voltage Ripple 233
- 8.3 Influence of Parasitics 234
- 8.3.1 Parasitic Capacitances 234
- 8.3.2 Finite On-Resistance 235
- 8.4 Charge Pump Implementation 235
- 8.4.1 Charge Pumps with Diodes 235
- 8.4.2 Charge Pumps with Transistor Switches 236
- 8.4.3 The Parasitic Bipolar Junction Transistor 238
- 8.5 Power Efficiency 239
- 8.6 Cascading of Pumping Stages 242
- 8.7 Other Charge Pump Configurations 243
- 8.8 Current-Source Charge Pumps 244
- 8.9 Charge Pumps Suitable as a Floating Gate Supply 245
- 8.10 Closed-loop Control 247 References 248

9 Capacitive DC-DC Converters 249

- 9.1 Introduction 249
- 9.2 Realizable Ratios 252
- 9.3 Switched-Capacitor Topologies 253
- 9.3.1 Series-Parallel 254

xii	Contents	
	9.3.2	Dickson 254
	9.3.3	Ladder 255
	9.3.4	Fibonacci 255
	9.3.5	Conclusion 256
	9.4	Gate Drive Techniques 256
	9.5	Charge Flow Analysis 257
	9.5.1	Charge Flow Vectors 257
	9.5.2	Charge Flow Vectors of Common Topologies 259
	9.5.3	Ideal Conversion Ratio 259
	9.5.4	Equivalent Output Resistance 261
	9.6	Output Voltage Ripple 267
	9.7	Topology Selection 268
	9.8	Capacitor and Switch Sizing 268
	9.8.1	Flying Capacitor Sizing 269
	9.8.2	Switch Sizing 270
	9.8.3	Output Capacitor Sizing 272
	9.9	Loss Analysis and Efficiency 273
	9.9.1	Intrinsic Losses 273
	9.9.2	Switch Control Losses 274
	9.9.3	Parasitic Capacitor Bottom-Plate Losses 274
	9.9.4	Static Losses 276
	9.9.5	Loss Minimization 276
	9.9.6	Total Losses 277
	9.9.7	Efficiency 277
	9.10	Multi-phase SC Converters 278
	9.11	Multi-ratio SC Converters 282
	9.11.1	Multi-ratio Implementation of Common SC Topologies
	9.11.2	Folding Dickson 284
	9.11.3	SAR SC Converters 285
	9.11.4	Recursive SC Converters 286
	9.12	Multi-phase Interleaving 290
	9.13	Control Methods 291
		References 293
	10	Inductive DC-DC Converters 297
	10.1	The Fundamental Buck Converter 297
	10.1.1	Inductor Current 298
	10.1.2	On-/Off-Times 298
	10.1.3	Volt-Second Balance 299
	10.1.4	Voltage Conversion Ratio 299
	10.1.5	Current Ripple 299
	10.1.6	Inductor Sizing 300
	10.1.7	Output Voltage Ripple 300
	10.1.8	Capacitor Sizing 301
	10.1.9	Switches 301
	10.1.10	Asynchronous Rectification 302
	10.2	Losses and Power Conversion Efficiency 302

283

Contents xiii

10.3 Closing the Loop 304 10.4 Hysteretic Control 305 10.5 Voltage-Mode Control (VMC) 306 10.5.1 Direct Duty Control 306 10.5.2 Voltage Feedforward 307 10.5.3 The Sawtooth Generator 308 10.5.4 The Error Amplifier 310 10.5.5 The Comparator 311 Closed-loop Transfer Function 312 10.5.6 Control-to-Output Transfer Function 312 10.5.7 10.5.8 Line-to-Output Transfer Function 313 10.6 Current-Mode Control (CMC) 313 Transfer Function of the Current Loop 315 10.6.1 10.6.2 Control-to-Output Transfer Function 316 10.6.3 The Initial Spike 316 Subharmonic Oscillations 317 10.6.4 10.7 Constant On-Time Control 322 10.8 Frequency Compensation 325 Compensator Types 325 10.8.1 10.8.2 Type I Compensator 325 10.8.3 Type II Compensator 326 Type III Compensator 327 10.8.4 10.8.5 The K-Factor Method 328 The K-Factor for Type II Compensation 10.8.6 328 The K-Factor for Type III Compensation 331 10.8.7 Capacitance Multiplier 333 10.8.8 10.9 Discontinuous Conduction Mode (DCM) 335 10.9.1 General Constant-Frequency Behavior 335 10.9.2 Pulse-Frequency Modulation (Burst Mode) 338 The Boost Converter 341 10.10 10.10.1 Inductor Current 341 Asynchronous Rectification 342 10.10.2 10.10.3 On-/Off-Times 342 10.10.4 Current Ripple 343 10.10.5 Inductor Sizing 343 Voltage Conversion Ratio 343 10.10.6 10.10.7 Output Voltage Ripple 344 10.10.8 Capacitor Sizing 344 10.10.9 Control Loop 344 10.10.10 The PWM Switch Model 345 10.10.11 Steady-State Analysis 347 10.10.12 Small-Signal Analysis 348 10.10.13 Control-to-Output Transfer Function 349 10.10.14 Right Half-Plane Zero (RHPZ) 349 10.10.15 Discontinuous Conduction Mode (DCM) 350 10.11 The Buck-Boost Converter 351 10.11.1 Inductor Current 352

- xiv Contents
 - 10.11.2 Asynchronous Rectification 352
 - 10.11.3 Voltage Conversion Ratio 352
 - 10.11.4 On-/Off Times 353
 - 10.11.5 Inductor Sizing 353
 - 10.11.6 Output Voltage Ripple and Capacitor Sizing 353
 - 10.11.7 Discontinuous Conduction Mode (DCM) 353
 - 10.11.8 Control-to-Output Transfer Function 354
 - 10.11.9 The Non-Inverting Buck-Boost Converter 355
 - 10.12 The Flyback Converter 356
 - 10.12.1 The Transformer 356
 - 10.12.2 Fundamental Operation 357
 - 10.12.3 Voltage Conversion Ratio 358
 - 10.12.4 Control-to-Output Transfer Function 358
 - 10.12.5 Control 358
 - 10.12.6 The Passive Clamp Flyback Converter (PCF) 358
 - 10.12.7 The Active Clamp Flyback Converter (ACF) 360
 - 10.13 Rectifier Circuits 360
 - 10.13.1 The Buffer Capacitor 361
 - 10.13.2 Low-Voltage Rectifier Circuits 362
 - 10.14 Multi-phase Converters 363
 - 10.14.1 Ripple Cancellation 364
 - 10.14.2 Design Choices 366
 - 10.14.3 Enhanced Transient Response 367
 - 10.14.4 Power Efficiency 367
 - 10.14.5 Phase Shedding 368
 - 10.14.6 Phase Balancing 368
 - 10.14.7 Coupled Inductors 371
 - 10.15 Single-Inductor Multiple-Output Converters (SIMO) 371
 - 10.15.1 Introduction 371
 - 10.15.2 Cross-Regulation 372
 - 10.15.3 Single Energizing Cycle per Switching Period 373 References 375

11 Hybrid DC-DC Converters 379

- 11.1 Hybridization of Capacitive and Inductive Concepts 380
- 11.2 The Benefit of Soft-Charging 381
- 11.2.1 Hard-Charging 381
- 11.2.2 Soft-Charging 383
- 11.3 Basic Resonant SC Converter Stages 385
- 11.4 Frequency Generation and Tuning 387
- 11.5 Equivalent Output Resistance 388
- 11.5.1 Equivalent Output Resistance at Resonance 389
- 11.5.2 *R_{out}* of the Fundamental 2:1 Hybrid Converter 390
- 11.5.3 Equivalent Output Resistance Over Frequency 391
- 11.5.4 Equivalent Output Resistance Diagram 394
- 11.6 Control of Hybrid Converters 394
- 11.6.1 Dynamic Off-Time Modulation (DOTM) 394

- 11.6.2 Pulse-Width Modulation (PWM) 396
- 11.6.3 Switch Conductance Regulation (SwCR) 396
- 11.6.4 Multi-Mode Operation 397
- 11.7 From SC to Hybrid Converters 398
- 11.7.1 Asymmetrical Phases 398
- 11.7.2 Analysis of the Soft-Charging Capability 399
- 11.7.3 Split-Phase Control 403
- 11.7.4 Boost Converters 405
- 11.8 Multi-phase Converters 405
- 11.9 Multi-Ratio Converters 406
- 11.10 The Three-Level Buck Converter 406
- 11.10.1 Pulse-Width Modulation 407
- 11.10.2 Switching Sequences 407
- 11.10.3 Voltage Conversion Ratio 408
- 11.10.4 Inductor Current and Output Voltage Ripple 408
- 11.10.5 Control of the 3L-Buck Converter 409
- 11.10.6 Flying Capacitor Balancing 410
- 11.10.7 An Implementation Example with V_{mid} -Generation 411
- 11.10.8 Start-up 412
- 11.11 The Flying-Capacitor Multi-Level Converter (FCML) 412
- 11.12 The Double Step-Down (DSD) Converter 414
- 11.12.1 General Operation 415
- 11.12.2 Inductor Current Balancing 417
- 11.12.3 Start-Up 417
- 11.13 Inductor-First Topologies 417 References 419

12 Physical Implementation 423

- 12.1 Layout Floor Planning 423
- 12.2 Packaging 424
- 12.2.1 Package Types 424
- 12.2.2 Bond Wires 426
- 12.2.3 Electrical Model 426
- 12.2.4 Thermal Behavior 427
- 12.2.5 System-in-Package 428
- 12.3 Electromagnetic Interference (EMI) 428
- 12.4 Interconnections 431
- 12.4.1 Classification 431
- 12.4.2 Continuous Current 431
- 12.4.3 High-d*i*/d*t* Loops 432
- 12.4.4 High-dv/dt Nodes 433
- 12.5 Pinout 433
- 12.6 IC-Level Wiring 435
- 12.6.1 Shielding 435
- 12.6.2 Grounding and Supply Connections 435
- 12.6.3 Thick Copper Metallization 437
- 12.7 PCB Layout Design 437

xvi Contents

- 12.8 Power Delivery 439
- 12.8.1 Lateral and Vertical Power Delivery 440
- 12.8.2 Integrated Voltage Regulators (IVR) 440
- 12.8.3 The Power Delivery Network (PDN) 441
- 12.9 Thermal Design 444
- 12.9.1 Thermal Resistance 444
- 12.9.2 Thermal Simulation 445 References 446

Index 449

Preface

In the March 2020 issue of the IEEE Solid-State Circuits Magazine, IEEE fellow Marcel Pelgrom writes in one of his excellent and inspiring Associate Editor's View columns entitled *Standing on Shoulders* about the timeless need for textbooks: "...where is the next disruptive view of our field, something that is desperately needed after this dazzling journey from 10-micron devices to nanometer electronics for quantum computing?" This book is my take on the field of power management.

The book delves into the fascinating world of power management IC design. This field has seen rapid growth in recent years, with the increasing demand for energy-efficient electronics, in particular, portable battery-operated devices. Power management integrated circuits are used for highly efficient power supplies and controlling power switches. It is incredible how these technologies have gained tremendous importance in making electronic solutions for global growth areas such as renewable energies, transportation, and communications more compact, energy-efficient, and reliable. Future machine learning and AI applications will only be possible with intelligent power management to supply complex processors and sensors.

I got into power management when I joined the industry in the early 2000s and went along a steep learning curve on all kinds of power management systems and design aspects. When I became a professor in 2010, I created a new course dedicated to power management IC design. However, no comprehensive textbook was available, and I had to rely on scientific papers and application notes.

A few years later, the idea of this book came up. Since then, I have been fascinated and challenged by the fast pace of progress and innovation in power management. The book provides a complete resource for those interested in power management IC design, covering basic concepts, advanced topics, and recent innovations in this rapidly evolving field. It is intended for students, educators, professors, and new and experienced engineers who want to learn about power management IC design, providing valuable insight and practical guidance for designing power management circuits and systems. Each chapter is organized to make it easy to find specific sub-topics, with numerous real-world examples illustrating key design concepts and techniques.

When I teach an entire course on power management IC design at a Master's or advanced Bachelor's level, I reduce the content and follow this outline: (1) Introduction (applications, challenges, physical implementation); (2) Linear Voltage Regulators; (3) Charge Pumps and Capacitive DC–DC Converters; (4) Power Transistors; (5) Gate Drivers; (6) Protection and Sensing; (7) Inductive DC–DC Converters; (8) Hybrid Converters. I also offer a design lab based on Spice simulation accompanying the lecture. Starting the class with the linear regulator right after the introduction allows the lab to begin early in the semester. I turned a lot of lab assignments and exercises into the many examples in this book (to my respected future students: I hope I'm not giving too much away.).

xviii Preface

In his column, Marcel Pelgrom also writes about the burden of writing textbooks. And indeed, this book is the result of an investment of uncountable hours over several years. Writing a book also means that there will be missing content, on purpose but also by mistake. My fellow readers: Despite careful review, there will be mistakes, and I apologize in advance. Any feedback is highly appreciated. Please get in touch.

This book would not be in your hands without careful review, invaluable feedback, and encouragement by many people. I want to thank my former and recent Ph.D. students, in particular, Peter Renz (who read through the entire draft) and Tobias Funk, Saurabh Kale, Maik Kaufmann, Tim Kuhlmann, Jens Otten, Christoph Rindfleisch, and Jürgen Wittmann. Thanks to Markus Henriksen for his feedback on switched-capacitor (SC) and hybrid converters. Hartmut Grabinski ensured that Maxwell's equations were correctly applied to interconnections and printed circuit board (PCB) layout. Detlev Habicht and Niklas Deneke supported in capturing photographs for the book. I am grateful to the team at Wiley, in particular, to Sandra Grayson, Juliet Booker, Kavipriya Ramachandran, and Jeevaghan Devapal for their excellent support and patience. I wish to thank many more people.

Writing such a book is impossible without the support of my family. I want to thank my parents, Siegrid and Eberhard, who have supported my fascination with microelectronic circuits since I was nine. Thanks go to my children, who became real fans of my book project, even though they often had to take a back seat, especially when finalizing the manuscript over the last 1–2 years. I am indebted to my wife, Sabine. This book would not have been possible without her love and understanding.

Enjoy the exciting journey of exploring the design of power management integrated circuits!

August 2023, Gehrden

Bernhard Wicht

1

Introduction

Power management integrated circuits (PMICs) are essential in today's electronic devices. They manage power delivery and consumption, provide efficient power supplies, and drive power switches that control actuators and motors, as illustrated in Fig. 1.1. PMICs can be integrated into complex integrated circuits (ICs) or implemented as dedicated ICs. In this book, the term PMIC will refer to any type of power integrated circuit.

The importance of PMICs has grown significantly in recent years, driving innovation and progress in various industries, from consumer electronics to automotive and industrial applications. With the progress of machine learning and artificial intelligence (AI), intelligent power management is critical to supplying complex processors and sensors.

PMICs have enabled the development of smaller, more energy-efficient, and reliable electronic solutions. They also play an essential role in environmental aspects and sustainability. By regulating the power supply of electronic devices, PMICs can reduce energy consumption and carbon emissions. Moreover, PMICs are crucial for the development of renewable energies, such as solar and wind power, by enabling efficient power conversion and management.

1.1 What Is a Power Management IC and What Are the Key Requirements?

A PMIC is an electronic component that delivers one or more supply voltages to other circuit blocks at a sufficient power level out of an electrical energy source, as shown in Fig. 1.1. The power conversion can happen in a linear way (usually the more straightforward method) or a switched-mode fashion, delivering energy portions at a specific frequency (usually the more energy-efficient approach).

The PMIC aims to utilize the energy source at maximum efficiency, while the input and output voltage may vary during operation. It also reacts to varying load currents from a few microamperes (standby) to several amperes (full-power operation).

The voltage conversion ratio is the relation V_{out}/V_{in} between the output and input voltage. The input voltage V_{in} can be greater or lower than the output voltage V_{out} , defining a step-down converter (buck converter) or a step-up converter (boost converter). Buck-boost converters allow V_{in} to vary over a wide range below and above V_{out} .

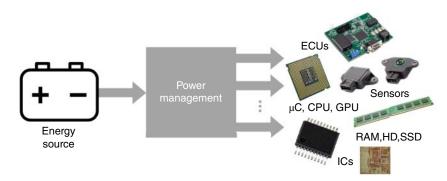


Figure 1.1 The role of power management: placed between the energy source and the electronics, it provides one or multiple supply voltages at the correct power level required by the application. Source: Brunbjorn/Adobe Stock; daniiD/Adobe Stock; Ruslan Kudrin/Adobe Stock; estionx/Adobe Stock.

The power conversion efficiency η (sometimes also called *PCE*) is defined as the ratio between the output power P_{out} delivered to the load and the input power P_{in} dissipated from the energy source,

$$\eta = \frac{P_{out}}{P_{in}} = \frac{P_{out}}{P_{out} + P_{loss}},\tag{1.1}$$

where P_{loss} accounts for the power dissipated within the power management circuit. It needs to be delivered from the input but does not contribute to the output power. We want to keep P_{loss} as low as possible. For $P_{loss} = 0$, the efficiency reaches its maximum, $\eta = 1$. It is common to express the efficiency in percent. In that case, we multiply Eqn. (1.1) by 100%.

PMICs typically include various features like voltage regulators, battery chargers, and power management control algorithms. They may also include monitoring and protection against overcurrent, overheating, and other failure cases. In some applications such as automotive, PMICs are alternatively called smart power ICs, emphasizing the combination of power devices with smart control and monitoring features, all integrated on a single chip.

One major trend is the increasing integration of PMICs. As more functions are combined onto a single chip, the resulting system becomes smaller, more efficient, reliable, and less expensive.

To summarize, the key requirements of PMICs are

- *Size, volume, footprint, and weight*: The PMIC, including external passive components, must often fit into a confined space like in smartphones or wearables. In portable devices, also the weight is critical. The lower weight is also crucial in automotive as it reduces gas and energy consumption.
- *Power conversion efficiency*: High efficiency means low losses. The lower the power losses, the longer the battery time. It also causes reduced heat and lower cooling effort, which, in turn, reduces the size and weight of the power management solution.
- *Reliability, no disturbances, and low noise*: PMICs are noise sources that may impact other sensitive electronic parts due to their switching nature. Handling high voltages and currents causes stress and reliability issues at the component, package, and assembly levels.
- *Cost*: Like most microelectronic products, there is always some pressure to reduce the cost of the IC and the overall bill of materials at the system level. Power management is not always considered a key differentiator. At the same time, physics cannot be cheated, and PMICs are a fastly growing market with good margins.

1.2 The Smartphone as a Typical Example

Looking at Fig. 1.2a), it is impressive to see how far mobile phones have come since the early 1990s. Back then, phones could only make voice calls and had a standby time of about a day or less. The picture is not to scale, but it was bulky and about 500 g in weight. It is incredible to think about all the features and functions that modern smartphones have today, illustrated in Fig. 1.2b). It is a remarkable example of the outstanding advancements in modern microelectronics. Today's smartphones are much smaller, lighter (typically 150 g), and more powerful. They have considerable computing power, 4K video capture, high-end gaming, virtual reality functions, and higher display resolution. This achievement in performance is thanks to ultra-low-power microelectronics and dedicated power management. Additionally, it is noteworthy that making a phone call is no longer the primary use case for these advanced devices.

Now we do what we usually do not want to; we drop our precious smartphone and look at the electronics inside. Figure 1.2c) shows a printed circuit board of the iPhone 13. The entire electronics is implemented on a layered motherboard sandwich of which Fig. 1.2c) shows a major part. The white frame boxes indicate some of the many PMICs inside the phone. There are more PMICs on the reverse side and other printed circuit board (PCB) parts, including ICs for the audio amplifier and wireless charging. PMICs are a considerable part of the smartphone. Connected to the Li-ion battery with a typical cell voltage of 3.7 V, multi-phase DC–DC converters supply the application processor that comprises multicore CPU and GPU blocks. The voltage levels are dynamically scaled in the range of typically 0.25–1.5 V at load currents of more than 10 A (see dynamic voltage and frequency scaling in Section 1.7). The typical power consumption is in the range of a few watts. In comparison, desktop PC processors dissipate more than 100 W. Running at high switching frequencies of tens of MHz, the voltage converters achieve small size, ultralow profile, and near-load integration at high conversion efficiency. No active cooling is required.

Looking closely, we identify hundreds of tiny passive components surrounding the ICs, mainly capacitors and inductors. As they are energy-storing components, their size can be reduced by decreasing the storing times, in other words, by increasing the switching frequency of the power conversion. It defines one of the leading research goals of today's power management solutions – achieving faster switching while keeping the conversion efficiency high. We will continuously address this topic throughout this book.



Figure 1.2 a) The mobile phone in the early 1990s, b) the smartphone today, and c) the electronics of the iPhone 13 with PMICs marked by white boxes. Source: a,b) aquatarkus/Adobe Stock; c) ifixit.

4 1 Introduction

1.3 Fundamental Concepts

There are different ways to implement DC–DC converters that convert an input DC voltage to another voltage level. To keep it more practical, we consider a scenario of how to convert 12 to 2 V.

1.3.1 Using a Resistor – The Linear Regulator

We can use a simple resistor to convert 12 to 2V, as shown in Fig. 1.3. For a load current of 1 A, a resistor of 10 Ω results in $V_{out} = 2$ V. In reality, the resistor is replaced by a controlled transistor such that its conductance is adjusted depending on the operating conditions like input voltage and load current. This approach works very well. However, the voltage drop between input and output is converted into heat. That is why there is significant power dissipation in the resistor, $10 \text{ V} \cdot 1 \text{ A} = 10 \text{ W}$ in this example. The power loss is even larger than the output power $P_{out} = 2$ W. In terms of energy efficiency, this concept has a significant drawback.

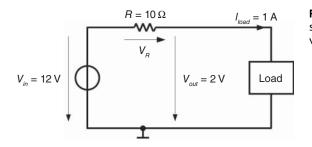
Nevertheless, it is the fundamental principle of a linear voltage regulator and, by far, the most used power management circuit today. On the positive side, besides its simplicity, it gives a "clean" output voltage with a fast transient response.

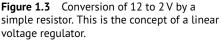
Without the excessive losses, there would be no need for alternative power conversion concepts, as discussed in Sections 1.3.2–1.3.4 below. The lower the voltage drop across the resistor (the controlled transistor), the lower the power loss. For this reason, linear regulators are often called low-dropout regulators with the widely used short-term LDO. Chapter 7 is dedicated to linear regulators.

1.3.2 Using Switches and an Inductor – The Inductive DC–DC Converter

To overcome the limited efficiency of the linear regulator, we again ask the question, how can we convert 12 to 2 V? We now use switches as shown in Fig. 1.4a). The switches are combined with an inductor, forming an inductive DC–DC converter as a typical switched-mode power supply (SMPS) implementation. As there is no resistive element in the power path, this concept has the potential to achieve much higher power conversion efficiency compared to a linear regulator.

The operation is as follows: The two switches turn on periodically in a complementary way. They are connected to the so-called switching node. The voltage V_{sw} at that node sees a square wave with an amplitude equal to V_{in} (12 V in this case), as shown in Fig. 1.4b). The switching node feeds into an L-C low-pass with two functions: filtering and energy storing. The filtering characteristic provides the average V_{sw} at the converter's output. The average corresponds to the area under the switching node transient curve. Hence, V_{out} is a DC voltage; see Fig. 1.4b). By changing the on-time t_{on} of S1, the area under the square wave, and, consequently, the level of V_{out} can be varied. This concept





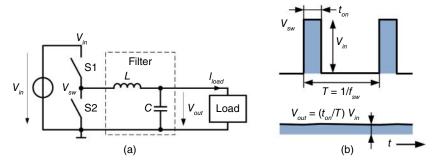


Figure 1.4 Voltage conversion using switches and an inductor *L* achieving high conversion efficiency: a) the fundamental step-down converter; b) waveforms of the switching node voltage V_{sw} and the output voltage V_{out} .

is called pulse-width modulation (PWM), the most popular control method in DC–DC converters. The duty cycle *D* defines the ratio between the on-time and the period time,

$$D = \frac{t_{on}}{T}.$$
(1.2)

For the step-down converter in Fig. 1.4, the duty cycle determines the voltage conversion ratio:

$$\frac{V_{out}}{V_{in}} = D = \frac{t_{on}}{T}$$
(1.3)

There are other topologies of DC-DC converters that have different conversion ratios.

The energy-storing characteristic of the L-C network is required in two ways. If S1 is turned on (S2 is off), energy is brought into the system. The capacitor C buffers V_{out} in case of varying load currents (load transients). C is called a bypass capacitor because it bypasses the actual regulator during instantaneous load steps before the control loop can respond. Alternatively, C is referred to as the output buffer capacitor. The inductor L delivers the load current if S1 is active and in the second switching phase when S2 turns on (S1 is off). Due to the switching nature of the DC–DC converter, there will always be some finite output voltage ripple. It is a significant disadvantage compared to linear regulators (Section 1.3.1). The ripple can be reduced by enlarging L and C at the expense of larger size and reduced power density. Another way of reducing the ripple and, at the same time, increasing the output power is to use multiple parallel DC–DC converters. Such multi-phase converters operate in a time-interleave scheme, delivering multiple energy packages during each cycle.

When discussing energy efficiency, it is essential to note that in a steady state, there should be no power loss P_{loss} at a switch. If the voltage across the switch is V and the current through the switch is I, the loss is $P_{loss} = V \cdot I$:

Switch turned on:
$$V = 0, I = I_{load} \rightarrow P_{loss} = V \cdot I = 0$$
 (1.4)

Switch turned off:
$$V = V_{max}, I = 0 \rightarrow P_{loss} = V \cdot I = 0$$
 (1.5)

 V_{max} is the (maximum) blocking voltage of the switch, which is equal to V_{in} in Fig. 1.4a). The relationship in Eqns. (1.4) and (1.5) is the fundamental reason, why switched-mode operation is widely used in power electronics. In actual designs, there will be various loss contributions, such as the finite on-resistance of the switches. There will also be switching losses and losses in the passive components. However, these losses are usually much lower compared to a linear regulator introduced in Section 1.3.1. Conversion efficiencies of more than 90% can be achieved. Chapter 10 covers inductive DC–DC converters comprehensively.

1.3.3 Switches and Capacitors – The SC Converter

Another way of voltage conversion is the combination of switches with capacitors. This concept has become very attractive for highly integrated power management designs due to the availability of high-density integrated capacitors in advanced CMOS technologies. Figure 1.5 shows a typical circuit along with the equivalent circuits in the two switching phases. During phase φ_1 , both capacitors are connected in series to V_{in} . The capacitors are parallel in phase φ_2 . The circuit periodically changes from a series to a parallel configuration, reducing the output voltage to half of the input voltage. Interestingly, this behavior is independent of the actual capacitor values. Their values determine the amount of charge shared between switching cycles, but in steady state, V_{out} will be exactly half of V_{in} . Note that ideally, no losses have occurred so far.

How can we convert 12 to 2 V? We can use two conversion stages. The first results in 6 V, the second one gives 3 V. How do we get to the target value of $V_{out} = 2$ V? We take advantage of the fact that C_1 can deliver only a limited charge. In other words, we let the load current discharge the output capacitor C until V_{out} reaches exactly 2 V. Most easily, this can be achieved by adjusting the clock frequency. Unfortunately, this is when the SC converter introduces power loss due to charge redistribution (~ CV^2). The output voltage drop from 3 to 2 V can be seen as a voltage drop across an equivalent output resistance. Significant research has been dedicated to finding improved SC converter topologies and control mechanisms that minimize these losses. SC converters are further explored in Chapter 9.

1.3.4 Switches and Capacitors and Inductors – The Hybrid Converter

This approach takes the SC converter of Fig. 1.5 and adds an inductor, as illustrated in Fig. 1.6. The combination of L and C leads to the name hybrid converter. It utilizes the benefits of the inductive and capacitive conversion concepts presented in Sections 1.3.2 and 1.3.3. Two mechanisms help improve conversion efficiency. The inductor ensures soft charging of the capacitor, which

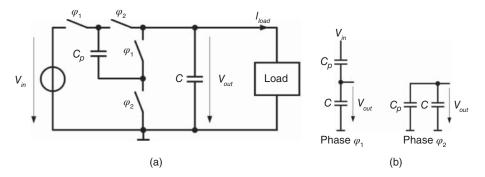


Figure 1.5 Voltage conversion using capacitors: a) the fundamental switched-capacitor voltage converter; b) the equivalent circuits in phases φ_1 and φ_2 , alternating between series and parallel configurations.

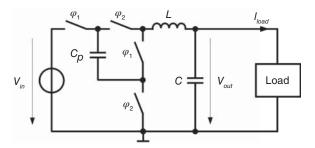


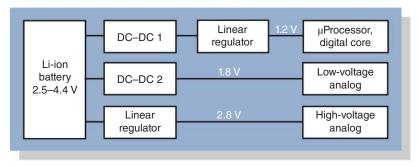
Figure 1.6 A hybrid converter formed by adding an inductor *L* to an SC converter resulting in higher conversion efficiency.

eliminates charge redistribution losses and minimizes the equivalent output resistance. L and C also form a resonant tank, which can achieve zero-current switching of the power switches. This way, the switching losses can be significantly reduced. On the downside, this concept has higher complexity than an inductive or capacitive converter. However, handling complexity is one of the great benefits of advanced microelectronics. Chapter 11 covers hybrid DC–DC converters comprehensively.

1.4 Power Management Systems

Electronic systems usually do not require only one supply voltage. Instead, various functional blocks have different supply voltage and power requirements. Figure 1.7 shows two examples of power management systems. Dedicated converters are assigned to supply each block at the point of load (PoL). State-of-the-art power management systems comprise multiple PoL regulators and DC–DC converters to supply microcontroller units (MCU), processors (CPU, GPU, and DSP), as well as analog and mixed-signal circuits.

In space-constraint applications such as smartphones, multiple voltage regulators are implemented in a single IC to minimize their footprint. Known as the multirail power supply (MRPS), it is the leading PMIC type with a market share of 20% (see Section 1.9).



(a)

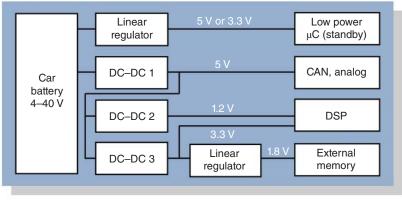




Figure 1.7 Point-of-load (PoL) power management systems: a) handheld devices operating from a Li-ion battery have lower step-down ratios as compared to b) automotive, industrial, and data center applications that operate from a higher supply voltage like a car battery.

8 1 Introduction

For large step-down ratios, linear regulators are not efficient. However, switched-mode DC–DC converters may not fulfill strict supply ripple and noise requirements for sensitive analog circuits such as sensor front ends. Hence, various conversion stages are combined, as illustrated in Fig. 1.7.

Combining a DC–DC converter as a first conversion stage with a subsequent linear regulator (LDO) is beneficial. The DC–DC converter guarantees high efficiency, while the LDO ensures a "clean" output voltage with a fast transient response. If the intermediate voltage V_{mid} , provided by the DC–DC converter, is close to the target output voltage, the linear voltage regulator will also show an acceptable efficiency. We can calculate the overall efficiency by multiplying the efficiency values of each stage:

$$\eta = \frac{P_{out}}{P_{in}} = \frac{P_{out}}{P_{mid}} \cdot \frac{P_{mid}}{P_{in}} = \eta_1 \cdot \eta_2$$
(1.6)

For a large step-down ratio, i.e., if V_{in} is much greater than V_{out} , achieving high efficiency will be more challenging.

As illustrated in Fig. 1.7a), a Li-ion battery typically supplies portable devices such as smartphones and wearables with a voltage range of 2.5–4.4 V. There is a moderate step-down ratio. The automotive application shown in Fig. 1.7b) operates from a 12 V lead-acid battery. The board net voltage can vary a lot, for instance, from 4 to 40 V. Hence, the step-down ratio is much larger than in devices supplied by a Li-ion battery. A step-up converter (boost converter) is typically inserted that kicks in if the board net drops toward 4 V and stabilizes the input voltage of the subsequent stages to typically 10 V (not shown in Fig. 1.7b) for simplicity). This way, the power management system can still provide 5 V at the output.

1.5 Applications

The application defines the energy source on the left of Fig. 1.1 with several examples shown in Fig. 1.8. Consequently, the applications also determine the system voltages, which are the power management input voltages. There is a trend toward higher voltages, as discussed in the following subsections, motivated by higher energy efficiency. For the same reason, the IC-level voltages of the electronics on the right of Fig. 1.1 scale into the opposite direction and reach levels of 1 V and lower. More details on IC-level supply voltages follow in Section 1.6. We discuss various applications below, starting with the lowest voltages at the bottom left of Fig. 1.8.

1.5.1 IoT Nodes and Energy Harvesting

Internet-of-Things (IoT) wireless nodes, installed in smart homes and office spaces and used in an industrial environment, are often designed with 10-year battery lifetime targets [1]. To prolong the life of a 3 V-CR2032 coin cell, the average current needs to be kept below 2.5 μ A (7.5 μ W). However, this can be challenging since the wireless node draws around 5 mA when it is in active mode (transmit). Several blocks contribute to this average power dissipation, including the CPU, the transceiver, sensors, and power management. Fortunately, continuous operation is not required, and duty cycling reduces the average current consumption to typically 6 μ A. The sleep current in the order of 1 μ A consists of leakage current, memory retention, analog circuits, such as a power-on reset, and a low-frequency sleep clock.

Energy harvesting can be used to expand the battery time. The ultimate goal is to remove the battery at all. In addition to the positive environmental impact, it can significantly reduce maintenance effort and cost. Besides the IC, the battery is the most expensive part of the wireless sensor

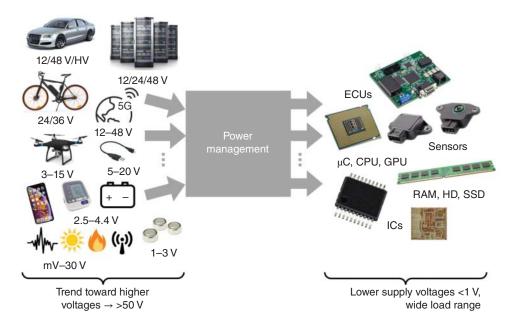


Figure 1.8 The system voltages in various applications define the input voltage for the power management circuits. On the load side, the supply voltages follow the trend of decreasing supply voltages toward 1 V and below with a wide load current range. Source: dezign56/Adobe Stock; ifeelstock/Adobe Stock; Pawinee/Adobe Stock; Scanrail/Adobe Stock, kornkun/Adobe Stock.

node (about 20% [1]). With the decreasing cost of the IC, the battery cost is expected to contribute a growing percentage of the total node cost over time.

Energy harvesting converts mechanical energy (kinetic energy and vibration), light (via solar cells), thermal energy, and the energy of radio frequencies (RFs) into usable voltages. RF energy harvesting is the lowest cost option, but the available power levels are the lowest. Hence, a promising approach is multisource energy harvesting. Nevertheless, the typical output power is in the order of 1 mW and below.

Power management circuits in energy harvesting applications operate from very low voltages in the millivolt range and even below. Charge pumps or similar techniques bring these low input levels to an intermediate voltage of \sim 0.5–1 V, just above the transistor threshold voltage. At this point, another step-up DC–DC converter (inductive or capacitive) kicks in. It boosts this voltage to 1.8 V, for instance, suitable for supplying functional electronic blocks. Once the voltage reaches the power-on reset level, the IoT node transmits a data packet and shuts off until enough power is available again.

1.5.2 Portable Devices, Smartphones, and Wearables

Many designs run from low-voltage batteries (button cells) in the range of 1-3 V. Li-ion batteries with a cell voltage of 2.5–4.4 V have become the primary battery technology for portable devices like laptops, mobile phones, and wearables. Laptops use two or three battery cells in series to supply input voltages of 7.4 or 11 V. Smartphones are covered as the introductory example in Section 1.2. The growing field of wearables includes applications like smartwatches, fitness trackers, smart headphones, glasses, medical monitoring devices, and implants. The power consumption of wearables is typically a few hundred milliwatts, an order of magnitude lower than a smartphone. It

10 1 Introduction

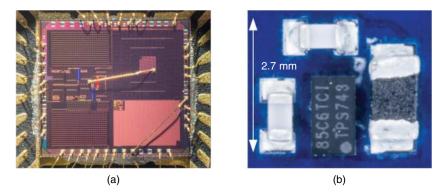


Figure 1.9 Miniaturized DC–DC converters for wearables: a) a fully integrated PMIC with on-chip integrated passives. Source: Peter Renz et al. [2]/from IEEE; b) A DC–DC converter in a 1.6 mm \times 0.9 mm, 8-ball wafer-level chip-scale package (WCSP) with discrete passives (TPS627431, Texas Instruments). Both photographs are depicted to scale. The size of the objects in the photographs is represented in relation to one another.

benefits from a smaller display with fewer pixels and a scaled-down CPU that runs at a lower frequency.

PMICs for portable devices must provide high power conversion efficiency to ensure long battery times. As the primary requirement, the PMIC designs need to be ultracompact and lightweight in addition to providing high power conversion efficiency. These advantages are achieved by fast-switching DC–DC converters with miniaturized passive components (see Section 1.8.3 and more details on integrated passives in Chapter 4).

Figure 1.9 shows two PMIC examples for wearables. Figure 1.9a) is a hybrid DC–DC converter with fully integrated passives [2]. The output buffer capacitor has a capacitance of 10 nF (lower right corner of the die photo), and the inductor is a square spiral coil of 9 nH (upper right, see Fig. 4.10 for an enlarged picture). Due to these small values, the converter operates at switching frequencies of up to 47.5 MHz. The power management circuits support low quiescent currents during sleep modes (power levels <25 mW) to achieve high efficiency and long battery times. The DC–DC converter in Fig. 1.9b) fits in a wafer-level chip-scale package (WCSP). The device is optimized to operate with a 2.2 μ H inductor and 10 μ F output capacitor, operating at 1.2 MHz. It offers ultralow quiescent current of typically 360 nA. Despite the compact design, the DC–DC converters in Fig. 1.9 reach peak efficiencies of more than 85% and 95%, respectively.

Example 1.1 We want to estimate the battery time of a smartwatch supplied by a Li-ion battery of 270 mAh. The battery voltage of $V_{bat} = 3.6$ V is converted to $V_{out} = 1.8$ V to supply the internal electronics at an output power of $P_{out} = 100$ mW. We distinguish two types of voltage conversion: a) an LDO (linear regulator) with an efficiency of 50%; b) a hybrid converter with an efficiency of 85%.

With an efficiency of less than 100%, the input power P_{in} will be higher than P_{out} . P_{in} determines the current drawn out to the battery. From Eqn. (1.1), we obtain for case a)

$$P_{in} = \frac{P_{out}}{\eta} = \frac{100 \text{ mW}}{0.5} = 200 \text{ mW},$$
(1.7)

$$I_{in} = \frac{P_{in}}{V_{in}} = \frac{200 \text{ mW}}{3.6 \text{ V}} = 56 \text{ mA}.$$
(1.8)