

GUANGYAO OUYANG | SHIJIE AN
ZHENMING LIU | YUXUE LI

COMMON RAIL FUEL INJECTION TECHNOLOGY IN DIESEL ENGINES



國防工業出版社
National Defense Industry Press

WILEY

Common Rail Fuel Injection Technology in Diesel Engines

Common Rail Fuel Injection Technology in Diesel Engines

Guangyao Ouyang

Naval University of Engineering
China

in collaboration with

Shijie An

Naval University of Engineering
China

Zhenming Liu

Naval University of Engineering
China

Yuxue Li

Naval University of Engineering
China

WILEY

 国防工业出版社
National Defense Industry Press

This edition first published in 2019 by John Wiley & Sons (Asia) Pte Ltd. under exclusive licence granted by National Defense Industry Press for all media and languages (excluding simplified and traditional Chinese) throughout the world (excluding Mainland China) and with non-exclusive license for electronic versions in Mainland China.

© 2019 National Defense Industry Press

All rights reserved. No part of this publication may be reproduced, stored in a retrieval system, or transmitted, in any form or by any means, electronic, mechanical, photocopying, recording or otherwise, except as permitted by law. Advice on how to obtain permission to reuse material from this title is available at <http://www.wiley.com/go/permissions>.

The right of Guangyao Ouyang, Shijie An, Zhenming Liu, and Yuxue Li to be identified as the authors of this work has been asserted in accordance with law.

This work is funded by B & R Book Program.

Registered Offices

John Wiley & Sons, Inc., 111 River Street, Hoboken, NJ 07030, USA

John Wiley & Sons Ltd, The Atrium, Southern Gate, Chichester, West Sussex, PO19 8SQ, UK

Editorial Office

The Atrium, Southern Gate, Chichester, West Sussex, PO19 8SQ, UK

For details of our global editorial offices, customer services, and more information about Wiley products visit us at www.wiley.com.

Wiley also publishes its books in a variety of electronic formats and by print-on-demand. Some content that appears in standard print versions of this book may not be available in other formats.

Limit of Liability/Disclaimer of Warranty

While the publisher and authors have used their best efforts in preparing this work, they make no representations or warranties with respect to the accuracy or completeness of the contents of this work and specifically disclaim all warranties, including without limitation any implied warranties of merchantability or fitness for a particular purpose. No warranty may be created or extended by sales representatives, written sales materials, or promotional statements for this work. The fact that an organization, website, or product is referred to in this work as a citation and/or potential source of further information does not mean that the publisher and authors endorse the information or services the organization, website, or product may provide or recommendations it may make. This work is sold with the understanding that the publisher is not engaged in rendering professional services. The advice and strategies contained herein may not be suitable for your situation. You should consult with a specialist where appropriate. Further, readers should be aware that websites listed in this work may have changed or disappeared between when this work was written and when it is read. Neither the publisher nor authors shall be liable for any loss of profit or any other commercial damages, including but not limited to special, incidental, consequential, or other damages.

Library of Congress Cataloging-in-Publication Data

Names: Ouyang, Guangyao, author. | An, Shijie, author.

Title: Common rail fuel injection technology in diesel engines / Guangyao

Ouyang, Naval University of Engineering, Wuhan ; in collaboration with, Shijie An, Naval University of Engineering, Wuhan, Zhenming Liu, Naval University of Engineering Wuhan, Yuxue Li, Naval University of Engineering, Wuhan.

Description: Hoboken, NJ : Wiley, 2019. | Includes bibliographical references and index. |

Identifiers: LCCN 2018057453 (print) | LCCN 2018057853 (ebook) | ISBN 9781119107248 (AdobePDF) | ISBN 9781119107262 (ePub) | ISBN 9781119107231 (hardcover)

Subjects: LCSH: Diesel motor--Fuel injection systems. | Marine diesel motors.

Classification: LCC TJ797 (ebook) | LCC TJ797 .O985 2019 (print) | DDC 621.43/61--dc23

LC record available at <https://lccn.loc.gov/2018057453>

Cover image: © Aun Photographer/Shutterstock

Cover design by Wiley

Set in 10/12pt WarnockPro by SPi Global, Chennai, India

Contents

Preface *xiii*

Introduction *xv*

1 Introduction *1*

- 1.1 The Development of an Electronic Control Fuel Injection System *2*
- 1.1.1 Position Type Electronic Control Fuel Injection System *3*
- 1.1.2 Time Type Electronic Control Fuel Injection System *4*
- 1.1.3 Pressure–Time Controlled (Common Rail) Type Electronic Control Fuel Injection System *4*
 - 1.1.3.1 Medium–Pressure Common Rail System *5*
 - 1.1.3.2 High–Pressure Common Rail System *6*
- 1.2 High–Pressure Common Rail System: Present Situation and Development *7*
- 1.2.1 For a Common Rail System *7*
 - 1.2.1.1 Germany BOSCH Company of the High–Pressure Common Rail System *8*
 - 1.2.1.2 The Delphi DCR System of the Company *10*
 - 1.2.1.3 Denso High–Pressure Common Rail Injection System of the Company *10*
- 1.2.2 High–Power Marine Diesel Common Rail System *11*
 - 1.2.2.1 System Structure *11*
 - 1.2.2.2 High–Pressure Oil Pump *12*
 - 1.2.2.3 Accumulator *13*
 - 1.2.2.4 Electronically Controlled Injector *13*

2 Common Rail System Simulation and Overall Design

Technology *15*

- 2.1 Common Rail System Basic Model *15*
 - 2.1.1 The Common Rail System Required to Simulate a Typical Module HYDSIM *16*
 - 2.1.1.1 Container Class *16*
 - 2.1.1.2 Valves *17*
 - 2.1.1.3 Runner Class Module *19*
 - 2.1.1.4 Annular Gap Class Module Physical Model Shown in Figure 2.6 *20*
 - 2.1.2 The Relevant Parameters During the Simulation Calculations *21*
 - 2.1.2.1 Fuel Physical Parameters *21*
 - 2.1.2.2 Fuel Flow Resistance *21*
 - 2.1.2.3 Partial Loss of Fuel Flow *22*

2.1.2.4	Rigid Elastic Volume Expansion and Elastic Compression	22
2.2	Common Rail System Simulation Model	23
2.2.1	High-Pressure Pump Simulation Model	23
2.2.2	Injector Flow Restrictor Simulation Model	24
2.2.3	Simulation Model Electronic Fuel Injector	25
2.2.4	Overall Model Common Rail System	25
2.3	Influence Analysis of the High-Pressure Common Rail System Parameters	26
2.3.1	Influence Analysis of the High-Pressure Fuel Pump Structure Parameters	26
2.3.1.1	Frequency of the Fuel Supply Pump	27
2.3.1.2	Quantity of the Fuel Supply by the High-Pressure Supply Pump	27
2.3.1.3	Diameter of the Oil Outlet Valve Hole of the High-Pressure Pump	29
2.3.1.4	Influence of the Pre-tightening Force of the Oil Outlet Valve	31
2.3.2	Analysis of the Influence of the High-Pressure Rail Volume	33
2.3.3	Influence of the Injector Structure Parameters	34
2.3.3.1	Control Orifice Diameter	34
2.3.3.2	Influence of the Control Chamber Volume	36
2.3.3.3	Influence of the Control Piston Assembly on the Fuel Injector Response Characteristics	36
2.3.3.4	Influence of the Needle Valve Chamber Volume	38
2.3.3.5	Influence of the Pressure Chamber Volume	38
2.3.3.6	Influence of the Nozzle Orifice Diameter on the Response Characteristics of the Injector	39
2.3.4	Influence of the Flow Limiter	40
2.3.4.1	Influence of the Plunger Diameter	40
2.3.4.2	Influence of the Flow Limiter Orifice Diameter	41
2.3.5	Common Rail System Design Principle	42
3	Electronically Controlled Injector Design Technologies	43
3.1	Electric Control Fuel Injector Control Solenoid Valve Design Technology	43
3.1.1	Solenoid Valve 33 Mathematical Analysis Model	43
3.1.1.1	Circuit Subsystem	43
3.1.1.2	Magnetic Circuit Subsystem	46
3.1.1.3	Mechanical Circuit Subsystem	47
3.1.1.4	Hydraulic Subsystem	48
3.1.1.5	Thermodynamic Subsystem	48
3.1.1.6	Dynamic Characteristic Synthetic Mathematical Model of the Solenoid Valve	49
3.1.2	Solenoid Magnetic Field Finite Element Analysis	49
3.1.2.1	Model Establishment and Mesh Creation	50
3.1.2.2	Loading Analysis	51
3.1.2.3	Result Display After ANSYS	53
3.1.3	Solenoid Valve Response Characteristic Analysis	53
3.1.3.1	The Influence of Spring Pre-load on the Dynamic Response Time of the Solenoid Valve	57

3.1.3.2	The Influence of Spring Stiffness on the Dynamic Response Time of the Solenoid Valve	60
3.1.3.3	The Influence of Driving Voltage on the Dynamic Response Time of the Solenoid Valve	60
3.1.3.4	Influence of Capacitance on the Dynamic Response Time of the Solenoid Valve	62
3.1.3.5	Influence of Structure of the Iron Core on the Response Characteristics of the Solenoid Valve	63
3.1.3.6	Influence of Coil Structure Parameters on the Response Characteristics of the Solenoid Valve	67
3.1.3.7	The Influence of Working Air Gap (Electromagnetic Valve Lift) of the Solenoid Valve	68
3.1.3.8	Material Selection of the Electromagnetic Valve	69
3.1.4	What Should Be of Concern When Designing the Solenoid Valve	71
3.2	Nozzle Design Technology	72
3.2.1	Mathematical Model and Spray Model Analysis of the Nozzle Internal Flow Field	72
3.2.1.1	CFD Simulation of the Nozzle Flow Field	73
3.2.1.1.1	Description of the Computational Model	73
3.2.1.2	Determination of the Calculation Area and Establishment of the Calculation Model	78
3.2.1.3	Discrete Computational Model of the Finite Volume Method	81
3.2.1.3.1	Computational Mesh Generation	81
3.2.1.3.2	Definition of Boundary and Initial Conditions	82
3.2.1.3.3	Numerical Solution	83
3.2.1.4	Spray Model of the Nozzle	84
3.2.1.4.1	Hole Type Flow Nozzle Model	85
3.2.1.4.2	WAVE Model	86
3.2.1.4.3	KH-RT Model	88
3.2.1.4.4	Primary Breakup Model of Diesel Engine	89
3.2.2	Analysis of the Influence of Injection on the Electronically Controlled Injector	90
3.2.2.1	The Effect of Injector Orifices	91
3.2.2.2	The Influence of the Ratio of the Length to the Diameter of the Orifice	95
3.2.2.3	The Influence of the Round Angle at the Inlet of the Orifice	101
3.2.2.4	The Influence of the Shape of the Needle Valve Head	106
3.2.2.5	Effect of the Injection Angle	110
3.2.2.6	The Influence of the Number of Orifices	116
3.2.3	Simulation and Experimental Study of Spray	119
3.2.3.1	Test Scheme	119
3.2.3.2	Simulation Calculation of the Nozzle Flow Field	119
3.2.3.3	Simulation and Test Verification of Spray	123
4	High-Pressure Fuel Pump Design Technology	127
4.1	Leakage Control Technique for the Plunger and Barrel Assembly	127
4.1.1	Finite Element Analysis of the Fluid Physical Field in the Plunger and Barrel Assembly Gap	130

4.1.1.1	Similarity Principle	130
4.1.1.2	Similarity Criterion	131
4.1.1.3	Dimensional Analysis and the Pion Theorem	132
4.1.1.4	Similarity Model and Finite Element Analysis of the Clearance Flow Field	133
4.1.2	Finite Element Analysis of the Plunger and Barrel Assembly Structure	138
4.1.2.1	Three-dimensional Solid Finite Element Model	138
4.1.2.2	Constraint Condition of Structure Field	139
4.1.2.3	Structural Field Solution	140
4.1.3	Structural Optimization of the Plunger and Barrel Assembly	140
4.1.3.1	Analysis of the Preliminary Simulation Result	140
4.1.3.2	Deformation Compensation Optimization Strategy	144
4.1.3.3	ANSYS Optimization Analysis	144
4.1.3.4	Evaluation of the Optimization Result	147
4.1.4	Experimental Study on the Deformation Compensation Performance of the Plunger and Barrel Assembly	148
4.1.4.1	Test for the Sealing Performance of the Plunger and Barrel Assembly	148
4.1.4.2	Plunger and Barrel Assembly Deformation Test	151
4.2	Strength Analysis of the Cam Transmission System for a High-pressure Fuel Pump	154
4.2.1	Dynamic Simulation of the Cam Mechanism of a High-Pressure Pump	155
4.2.1.1	Solid Modeling	155
4.2.1.2	Rigid-Flexible Hybrid Modeling and Simulation of the Camshaft Mechanism	156
4.2.2	Stress Analysis of the Cam and Roller Contact Surface	158
4.2.2.1	Contact Stress Calculation Method	159
4.2.2.2	Calculation of Contact Stress under the Combined Action of Normal and Tangential Loads	162
4.2.2.3	Analysis of the Cam Working State	164
4.2.3	Experimental Study on Stress and Strain of the High-Pressure Fuel Pump	169
4.2.3.1	Test and Analysis of the Pressure of the Plunger Cavity	169
4.2.3.2	Stress Test and Analysis of the Camshaft	174
4.3	Research on Common Rail Pressure Control Technology Based on Pump Flow Control	176
4.3.1	Design Study of a High-Pressure Pump Flow Control Device	177
4.3.1.1	Overview of a High-Pressure Pump Flow Control Device	177
4.3.1.2	Structure and Working Principle of the High-Speed Solenoid Valve	181
4.3.1.3	Simulation of the Static Characteristic of the Solenoid Valve	183
4.3.1.4	Simulation of Dynamic Characteristics of the Solenoid Valve	188
4.3.1.5	Design and Optimization of the One-Way Valve	191
4.3.2	Conjoint Simulation Analysis of a Flow Control Device and the Common Rail System	194
4.3.2.1	Simulation of the Flow Control Device	194
4.3.3	Analysis of Simulation Results	196
4.3.4	Experimental Study on the Regulation of Common Rail Pressure by the Flow Control Device	200

- 4.3.4.1 Test Device 200
- 4.3.4.2 Sealing Performance Test of the One-Way Valve 201
- 4.3.4.3 Experimental Study on the Dynamic Response Characteristics of the Electromagnet 202
- 4.3.4.4 Test of Pressure Control in the Common Rail Chamber 204
- 4.3.4.5 Test Results 205
- 4.3.4.6 Experimental Study of the Influence of the Duty Ratio of the Solenoid Valve on the Pressure Fluctuation of the Common Rail 208

- 5 ECU Design Technique 211**
- 5.1 An Overview of Diesel Engine Electronically Controlled Technology 211
- 5.1.1 The Development of ECU 212
- 5.1.1.1 The Application of Control Theory in the Research of an Electronically Controlled Unit 212
- 5.1.1.1.1 Adaptive Control and Robust Control 212
- 5.1.1.1.2 Neural Network and Fuzzy Control 213
- 5.1.1.2 Function Expansion of the Engine Management System 213
- 5.1.1.2.1 Fault Diagnosis Function for an Electronically Controlled Engine 214
- 5.1.1.2.2 Field Bus Technology 214
- 5.1.1.2.3 Sensor Technology 214
- 5.1.1.3 Development of Computer Hardware Technology 215
- 5.1.2 Development of Electronically Controlled System Development Tools and Design Methods 215
- 5.1.2.1 Application of Computer Simulation Technology 215
- 5.1.2.2 Computer-Aided Control System Design Technology 216
- 5.2 Overall Design of the Controller 217
- 5.2.1 Controller Development Process 217
- 5.2.2 Hierarchical Function Design and Technical Indicators of the Controller 219
- 5.2.3 Input Signal 221
- 5.2.3.1 Man–Machine Interactive Interface Input Signal 222
- 5.2.3.1.1 Switching Signal 222
- 5.2.3.1.2 Continuous Signal 222
- 5.2.3.2 Sensor Input Signal 222
- 5.2.3.2.1 Temperature Input Signal 222
- 5.2.3.2.2 Pressure Input Signal 223
- 5.2.3.2.3 Pulse Input Signal 223
- 5.2.4 Output Signal 223
- 5.2.4.1 Starting Motor Control Switch Signal 225
- 5.2.4.2 Drive Signal of the Electronically Controlled Injector 225
- 5.2.4.2.1 Time Precision Requirements 225
- 5.2.4.2.2 Current Waveform Requirements 226
- 5.2.4.2.3 Power Requirements 226
- 5.2.4.3 The Driving Signal of the Solenoid Valve Controlled by the Common Rail Chamber Pressure 227
- 5.3 Design of the Diesel Engine Control Strategy Based on the Finite State Machine 228

5.3.1	Brief Introduction of the Finite State Machine	228
5.3.1.1	Finite State Machine Definition	228
5.3.1.2	State Transition Diagram	229
5.3.2	Design of the Operation State Conversion Module	229
5.3.3	Design of the Self-Inspection State Control Strategy	232
5.3.4	Design of the Starting State Control Strategy	232
5.3.5	Design of a State Control Strategy for Acceleration and Deceleration	233
5.3.6	Design of a Stable Speed Control Strategy	234
5.3.7	Principle of the Oil Supply Pulse	234
5.4	Design of the ECU Hardware Circuit	235
5.4.1	Selection of Core Controller Parts	235
5.4.1.1	Characteristics of FPGA	236
5.4.1.2	Selection of Core Auxiliary Devices	237
5.4.2	Control Core Circuit Design	238
5.4.2.1	FPGA Circuit Design	238
5.4.2.1.1	Power Supply Design	239
5.4.2.1.2	Configuration Circuit Design	239
5.4.2.1.3	Logic Voltage Matching Circuit	239
5.4.2.2	Circuit Design of SCM	240
5.4.3	Design of the Sensor Signal Conditioning Circuit	242
5.4.3.1	Design of the Signal Conditioning Circuit for the Temperature Sensor	242
5.4.3.2	Design of the Signal Conditioning Circuit for the Pressure Sensor	244
5.4.3.3	Design of the Pulse Signal Conditioning Circuit	245
5.4.4	Design of the Power Drive Circuit	248
5.4.4.1	Design of the Power Drive Circuit of the Pressure Controlled Solenoid Overflow Valve in the Common Rail Chamber	248
5.4.4.2	Design of the Power Drive Circuit for the Solenoid Valve of the Injector	249
5.5	Soft Core Development of the Field Programmable Gate Array (FPGA)	255
5.5.1	EDA Technology and VHDL Language	256
5.5.1.1	Introduction of EDA Technology and VHDL Language	256
5.5.1.2	Introduction of EDA Tools	257
5.5.2	Module Division of the FPGA Internal Function	258
5.5.3	Design of the Rotational Speed Measurement Module	261
5.5.3.1	Measuring Principle	261
5.5.3.2	Structure Design	263
5.5.4	Design of the Control Pulse Generation Module for the Injector	266
5.5.4.1	The Function, Input, and Output of the Injector Control Pulse Generation Module	266
5.5.4.1.1	Shortening Timing Compensation Method	268
5.5.4.1.2	Increasing the Advance Angle Compensation Method	269
5.5.4.2	The Realization of the Control Pulse Generation Module of the Injector	271
6	Research on Matching Technology	273
6.1	Component Matching Technology of the Common Rail System	273
6.1.1	Matching Design of the High-Pressure Fuel Pump	273
6.1.2	Matching Design of the Rail Chamber	274
6.1.3	Matching Design of the Injector	274

6.1.3.1	Modeling and Verification of Diesel Engine Spray and the Combustion Simulation Model	276
6.1.3.2	Optimal Parameters and Objective Functions	278
6.1.3.3	Simulation Experiment Design (DOE)	278
6.1.3.4	Establishment of an Approximate Model for the Response Surface	280
6.2	Parameter Optimization and Result Analysis of the Injection System	281
6.2.1	DoE Optimization	281
6.2.2	Global Optimization Based on the Approximate Model	282
6.2.3	Optimization Results Analysis	283
6.3	Optimization Calibration Technology of the Jet Control MAP	285
6.3.1	Summary	285
6.3.2	Optimal Calibration Method	285
6.3.3	Optimization of Target Analysis	286
6.4	Off-line Steady-State Optimization Calibration of the Common Rail Diesel Engine	286
6.4.1	Mathematical Model for Optimization of the Electric Control Parameters	287
6.4.2	Experimental Design	287
6.4.3	Establishment of the Performance Prediction Response Model	288
6.4.4	Optimal Calibration	289
6.4.5	Test Result	291
7	Development of the Dual Pressure Common Rail System	293
7.1	Structure Design and Simulation Modeling of the Dual Pressure Common Rail System	295
7.1.1	Design of the Dual Pressure Common Rail System Supercharger	295
7.1.2	Modeling of the Dual Pressure Common Rail System	299
7.2	Simulation Study of the Dual Pressure Common Rail System	299
7.2.1	Study of the Dynamic Characteristics of the System	299
7.2.1.1	Simulation of the Dynamic Characteristics of the System	300
7.2.1.2	Sensitivity Analysis of the Structural Parameters of the Supercharger	303
7.2.1.3	Study on Pressure Oscillation Elimination of the Supercharger Chamber in the Dual Pressure Common Rail System	308
7.2.1.3.1	Scheme I	309
7.2.1.3.2	Scheme II	311
7.2.2	Prototype Trial Production	312
7.3	Control Strategy and Implementation of the Dual Pressure Common Rail System	313
7.3.1	Control Strategy of the Dual Pressure Common Rail System	314
7.3.2	Hardware and Software Design of the Controller Based on the Single Chip Microcomputer	315
7.3.2.1	The Basic Composition of the Control System	315
7.3.2.2	Performance of Control Chip and Its Circuit Design	316
7.3.2.2.1	The Circuit Design of the Minimum System of the Single Chip Microcomputer	316
7.3.2.2.2	Design of the Serial Communication Circuit	316
7.3.2.2.3	Pulse Signal Conditioning Circuit	318

- 7.3.2.3 Programming of Control System 319
- 7.3.3 Drive Circuit Design 319
 - 7.3.3.1 Design Requirements of the Driving Circuit 319
 - 7.3.3.2 Design of the Power Drive Circuit 321
 - 7.3.3.2.1 Power Drive Circuit of the GMM Actuator 321
 - 7.3.3.2.2 Power Drive Circuit of the Solenoid Valve 323
- 7.4 Experimental Study on the Dual Pressure Common Rail System 325
 - 7.4.1 Test of Pressurization Pressure and Injection Law 325
 - 7.4.1.1 Test Platform for Pressurization Pressure and Fuel Injection 325
 - 7.4.1.2 Simulation and Test 328
 - 7.4.1.3 Effect of the Turbocharging Ratio on Pressure and Fuel Injection Law 329
 - 7.4.1.4 Effect of the Control Time Series on Pressurization Pressure and Fuel Injection Law 334
 - 7.4.1.5 Test of System High-Pressure Oil Consumption 334
 - 7.4.2 Test on Spray Characteristics of the Dual Pressure Common Rail System 336
 - 7.4.2.1 Spray Photography Test Platform 336
 - 7.4.2.2 Effect of the Fuel Injection Law on Fuel Injection Quantity 338
 - 7.4.2.3 Effect of the Injection Rate Shape on Spray Penetration and the Spray Cone Angle 338
 - 7.4.3 Experimental Research Conclusions 340

Index 343

Preface

Since the twenty-first century, the diesel engine is facing the challenge of two factors: energy and environmental protection; thus improving the efficiency and controlling the emissions has become an important problem facing today's diesel engine industry. The needs of society and economy of the diesel engine for future environmental protection put forward a higher request for better technology to enable a lift in demand for the diesel engine. The efficiency and lower emissions are closely related to the combustion process. The most feasible approach is to reform the diesel engine fuel system implementation to improve its performance. The electronically controlled fuel injection technology is an implementation of controlling the fuel injection quantity, injection timing, and fuel injection law, in order to realize the well-organized combustion process and optimize performance of economy, power, and emission under various working conditions.

Development of the electronic control fuel injection technology began in the 1970s, and the actual shipment of electronically controlled high-power diesel engines started to be commissioned in 1980. So far, the electronically controlled fuel injection system has passed through three stages of development: the initial development stage in 1970s, the production utility stage in the 1980s, and the stage of technological development in the 1990s. Currently, the most advanced electronic control fuel injection technology is the high-pressure common rail fuel injection technology.

The first generation of a common rail system was launched in the 1990s, with the second and third generations being rolled out after more than 10 years of research and improvement. The concept of a fourth generation of common rail system has been promoted in recent years. The latest mid-high speed and high-power diesel engines developed abroad, with no exception, adapted the common rail technology, so it is apparent that the common rail technology has become one of the important technical measures to respond to emissions and fuel economy.

Although common rail technology is one of the hot topics in the study of the modern diesel engine technology with abundant successful application examples, the system study is relatively rare, and it especially lacks a domestic research report. The author has been engaged in the research of this field for more than 10 years, involving research and development stages of demonstration, design, and key technology research. The author has reached a series of achievements with arduous effort and suffered from a deficiency of system data; thus he has developed the germination of summing up the research achievements systematically over the years, to offer some reference for

colleagues. It is his wish to provide a bit of inspiration and hopes that it might make a contribution to diesel engine technology development.

This book is based on the perspective of system analysis in order to provide a comprehensive introduction to common rail technology. The book is divided into seven chapters: the first chapter analyses the present situation of the common rail system; the second chapter introduces the common rail system modeling and simulation technology; the third and fourth chapters introduce the research of key technology and key parts of the common rail system; the fifth chapter introduces the ECU design technology; the sixth chapter introduces the machine assembling technology of the common rail system; and the seventh chapter introduces the research and development of a new type of common rail system.

The book is available for senior students in relevant colleges for graduate teaching and engineering and technical personnel. Due to a possible limited level of knowledge of the author, the book offers a preliminary view; if there are some inappropriate statements, please correct them.

The author gratefully acknowledges the help of Professor Jiang Deming at Xi'an Jiaotong University, Professor Gao Xiaohong at Wuhan University of Science and Technology, with the guidance and recommendation of Professor Wang Changyi and Professor Tang Kaiyuan at Naval Engineering University. Thanks also for the support of the National Defense Industry Press. Thanks also to colleagues and graduate students for 10 years of hard work, and it is their support that provided the author with the determination and confidence to realize the publication of this book.

The author

Introduction

This book is the academic monograph about related technical aspects of the high-pressure common rail system of a diesel engine and summarizes the author's research achievements in the field of electronic injection and common rail technology in the past decade. This book systematically elaborates the following contents: the development history of high-pressure common rail technology, system simulation and optimization, key parts design and the optimization design of a new type of common rail technology, etc.

This book can be used as a reference book for Graduate teaching and is also available for engineering and technical personnel specializing in design, development, and manufacture of a common rail system of a diesel engine.

1

Introduction

Today, the diesel engine is being developed and perfected; with its advantages of high efficiency and a wide range of power, it has been widely used in industry, agriculture, national defense, and other fields. Predictably, the diesel engine will still occupy an important position in the field of engines for a long time in the future. With increasingly serious energy and environmental problems, people pay more and more attention to fuel economy and emissions of the diesel engine, especially putting emission issues at the top of considerations. Governments have developed increasingly stringent emission regulations since the 1970s, and internal combustion engine researchers and related companies have constantly committed to improve the performance of the diesel engine, in order to obtain better noise emissions and a more economic performance.

There are many factors that influence diesel engine exhaust emissions and fuel economy, which are quite complicated. The most important means of improving the emissions and economic performance of diesel engine performance is to improve its combustion performance. Therefore, transformation of the fuel injection system has become an object of primary concern since it has the greatest influence on the combustion performance. The parameters that impact the performance of the diesel fuel injection system mainly include injection pressure, injection quantity, fuel injection advance angle, etc. Traditional methods are not able to make these parameters in the diesel engine achieve optimal results in the broad scope of work carried out on the diesel engine, but the development of modern electronic technology has provided a broad space in which to improve the performance of the diesel engine.

The biggest impact of the diesel engine fuel injection system on combustion concerns three factors: injection timing, injection duration, and the fuel injection law. The main purpose of an electric controlled diesel engine fuel injection system is to realize the flexible adjustment of the above three factors, which ensure that the diesel engine is running in optimal working conditions.

The diesel engine electronic control injection system is usually composed of sensors, controllers, and actuators, as shown in Figure 1.1. The combustion process in the cylinder of the diesel engine is very complex, and is affected by many factors. The method of setting up a mathematical model, with the aid of all kinds of sensors, to realize the closed-loop control of the burning process is difficult. The basic method that most diesel engine electronic control fuel injection systems now adopt is: adopting engine speed and load as a basic signal reflecting the actual working conditions of the diesel engine; then referring to the fuel injection quantity obtained by experiment in the optimum working condition and the injection timing MAP graph in order to determine the basic

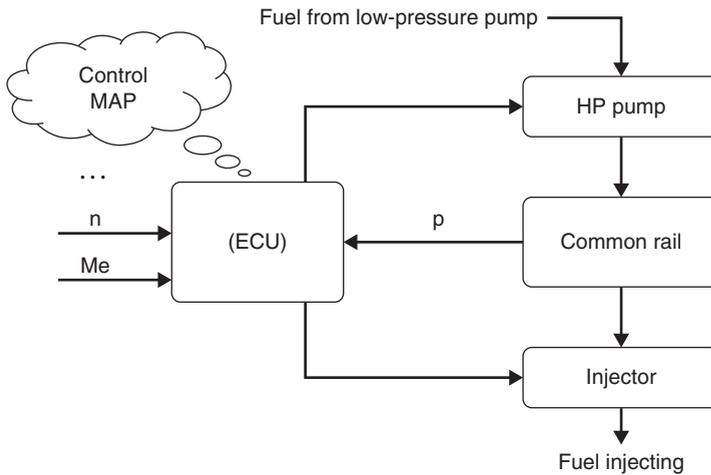


Figure 1.1 The basic compositions of the fuel injection system on an electronic controlled diesel engine.

fuel injection quantity and injection timing; then carrying on the various compensation schemes (such as engine speed, load, water temperature, oil temperature, atmospheric pressure, etc.) in order to determine the cycle fuel injection quantity and injection timing; and then taking the closed-loop feedback control to actuators in the process of working.

After the diesel engine fuel system adopts the electric control system, it has the following features:

- (1) The degree of control freedom increases. The electronic control fuel injection system can optimize comprehensive control on the injection parameters in accordance with the different operating conditions.
- (2) The control precision improves. For instance, the injection timing control accuracy (CA) is higher than 0.5° CA and the accuracy is four times higher than with mechanical control.
- (3) Since the diesel engine fuel injection system has the characteristics of high voltage and high frequency and pulse, it will be able to achieve these objectives and will certainly bring about the complexity of actuator and control and strict requirements on reliability and duration of system that are required.

1.1 The Development of an Electronic Control Fuel Injection System

After decades of development, the diesel engine electronic control fuel injection system has experienced three progressive stages, namely, position type control, time control, and pressure time control.

Table 1.1 Typical representatives of a position type electronic control fuel injection system.

Form	System name	Control characteristics
S T	Pump Zexel (Japan) COPEC	High-speed solenoid valve control injection time, variable inductance displacement control fuel injection quantity
R A	BOSCH (Germany company) EDR	High-speed solenoid valve control gear lever displacement, adjustable CAM phase
I G	(American Caterpillar company) PEEC – ECD-P3	Brushless torque motor control gear lever displacement, linear potentiometer control injection time
H	(Japan Toyota) ECD-p	High-speed solenoid valve control injection time, adjustable CAM phase
T	BOSCH (Germany company) TICS	High-speed solenoid valve control plunger sleeve and gear lever position, the variable stroke
C	(Japan Toyota) ECD-p	High-speed solenoid valve control injection time, adjustable CAM phase
O	(British Lucas) EPIC	The phase of the CAM ring to control injection timing, control the distribution of rotor axial displacement control of oil
L U	(Stanadyne companies in the United States) PCF	Control CAM follower body axial displacement control of oil, the control of fuel injection advance unit control injection time
M N	BOSCH (Germany company) ECD – COVEC	Rotating magnet control sliding sleeve position, solenoid valve control injection time

1.1.1 Position Type Electronic Control Fuel Injection System

A position type electronic control fuel injection system retains the basic structure of a traditional injection system and only replaces the original mechanical control mechanism with electronic components. On the basis of the original mechanical control loop fuel injection quantity and injection timing, the electromagnetic actuator of linear displacement or angular displacement has been adapted to realize electrically controlled fuel injection timing and to improve control accuracy and the mechanical control response speed. Its products involve an array plunger pump electronic control system and a rotor pump distribution electric control system. Typical representative types are shown in Table 1.1.

A position type electronic control injection system adapts electronic control components to replace the original mechanical adjusting mechanism, while the use of electronic control mechanical actuators is to control the process of injection indirectly; thus the control accuracy, response time, is comparatively lower than in other electronic control systems. Since the basic structure of the injection system has not changed, the injection characteristics cannot be greatly changed and so the injection rate is not likely to achieve flexible control.

1.1.2 Time Type Electronic Control Fuel Injection System

As the performance of the diesel engine has further requirements on fuel injection process control, the first generation of fuel injection systems that installed an electronic control device with the original mechanical injector could not meet demand and thus the second generation of electronic control fuel injection system arises at the historic moment to use the electronic control unit (ECU) to control the injection starting point and end point directly. It has changed the traditional injection system of some mechanical structures, switching the original mechanical injector to a high-speed powerful solenoid valve injector, controlling the make and breaks of the electromagnetic valve through a pulse signal, and the action controls the opening and closing of the oil atomizer. The oil pump is completely separated from this mechanism and the control mechanism, and fuel metering is determined by the fuel valve open time length and the size of the injection pressure. Injection timing is controlled by the electromagnetic valve open time, in order to realize flexible control of the fuel injection quantity, injection timing, and the integration of control. It has changed the execution of the first generation of electronic control fuel injection systems, such as a slow response, low control frequency, and unstable control precision, and thus has much greater control of the degrees of freedom and a better control performance, which the first generation of the electric control system cannot reach. The electric control system can be divided into: an electric pump nozzle system, an electric distribution pump system, and an ECU pump or inline pump system. Typical representatives are shown in Table 1.2. Though the performance has improved greatly, it still has the following disadvantages: since the injection pressure is produced by a high-pressure oil pump directly, the injection pressure and fuel injection law is still under the control of the CAM (computer aided manufacture)-shaped line and cannot be adjusted freely.

1.1.3 Pressure–Time Controlled (Common Rail) Type Electronic Control Fuel Injection System

All the electronic control fuel injection systems described above directly adopt the traditional mechanical fuel pump pressure oil and fuel injection mechanism, with its basic principle based on fuel injection pump technology developed by Robert Bosch in 1926.

Table 1.2 Time control type electronic control fuel injection system.

Form	System name	Control characteristics
Pump nozzle	Detroit Diesel Engine Company (DDEC)	Solenoid valve open and close control injection start and end
	British Lucas EUI	As above
	The University of Tokyo in Japan ACE	As above
Distribution pump	Zexel Japanese company ECD-V3	With oil spill control valve adjustment of oil pump
	DS (Stan dyne companies in the United States)	RS with high-speed solenoid valve control oil injection time and quantity
	Germany BOSCH company VP44	As above

In order to meet increasingly stringent needs of emission, noise regulations, and fuel consumption reduction, it must improve the control precision of the fuel injection quantity, injection timing, and fuel injection rate, in order to obtain fine control of each cylinder and adopt the high-pressure jet to get a better atomization effect. All these requirements prompted production of the third generation of electronic control fuel systems, that is, the emergence of the common rail electronically controlled fuel injection system.

The common rail system is characterized by: independent generation of the injection pressure and injection control and pressurization of the fuel in the common rail using a fuel supply pump in which the pressure can be maintained within the scope of 130–160 MPa, although some related research reports claim that it has reached 200 MPa. The opening and closing of the electromagnetic valve control the start and end of the fuel injection process. Thus, it can change the injection pressure according to the engine load and speed, with an operation condition in a wide range of 20–160 MPa, realizing the pilot injection, main injection, multistage spray, etc. It can also change the shape of the fuel injection rate in accordance with the demand, realize a high degree of freedom to control the fuel injection process, greatly improve the combustion efficiency of the diesel engine, and significantly improve emission performance.

The common rail fuel injection system formally entered the stage of practical application in the middle and later periods in the 1990s. This kind of electric control system can be divided into: an electronically controlled medium-pressure common rail fuel injection system (hereinafter referred to as the medium-pressure common rail system) and the electronically controlled high-pressure common rail fuel injection system (hereinafter referred to as the high-pressure common rail system).

1.1.3.1 Medium-Pressure Common Rail System

The fuel pressure in the fuel rail of a medium-pressure common rail system is 525 MPa. The fuel with medium pressure is sprayed into the combustion chamber using fuel injector booster piston pressurization with extremely high pressure. The typical representatives are the Servojet system by the BKM Company and the HEUI system by the Caterpillar Company.

The structure diagram of the HEUI system by the Caterpillar Company is shown in Figure 1.2. This system adapts a pressurization piston with the aid of machine oil pressure to increase the injection pressure and has two public oil ways. One is a high-pressure control oil way (the high-pressure control oil is machine oil), maintaining a certain degree of pressure to push a supercharging piston. Another is the low-pressure fuel oil supply, which provides fuel for the fuel injector. It controls the fuel injection pressure by adjusting the oil pressure in a high-pressure control oil circuit. Fuel injection quantity and injection timing are controlled by the solenoid valve open time length and opening moment.

The main characteristics of the system are as follows:

- A. A very high injection pressure may be obtained by changing the proportion of pressure of the piston and plunger of the cross-section area.
- B. High pressure only exists in the necessary part (booster amplifier, high-pressure tubing, etc.).
- C. It does not need a high-pressure oil pump.

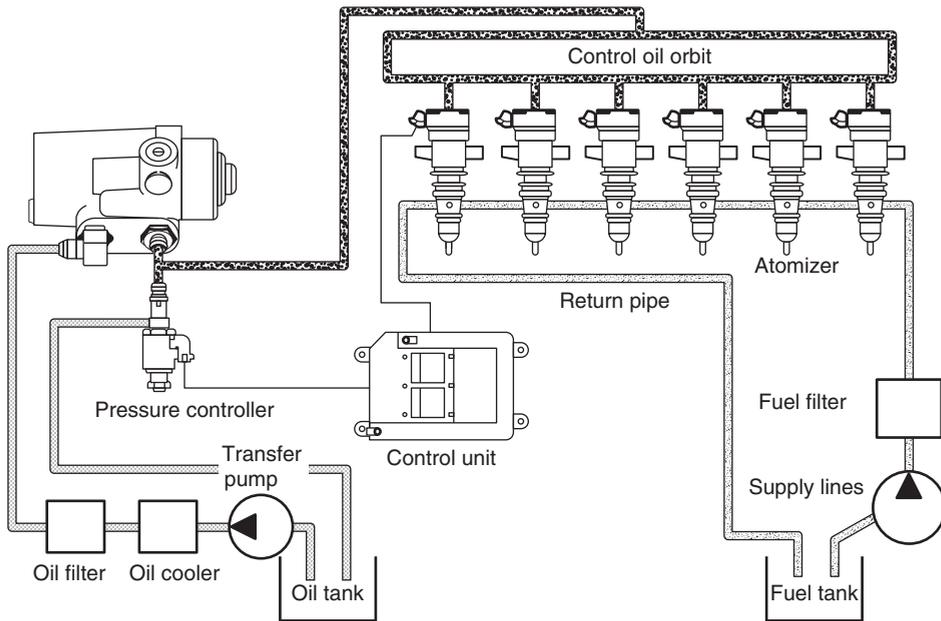


Figure 1.2 Schematic diagram of the liquid pressure type electronic control fuel injection system.

- D. The injection shape is affected. It must adopt a large-flow electromagnetic valve (such as where the pressure ratio is 7 : 1 and the circulating oil quantity is more than seven times that of each injection volume). Since the response speed of the large-flow electromagnetic valve is comparatively slow, it is not easy to achieve advance injection when the injection time is very short.
- E. Its installation size is comparatively large and it needs two sets of oil ways so that the oil duct size is also bigger.
- F. It needs fuel valve plunger parts with high precision in order to ensure the separation of the high-pressure oil and jet fuel control.

1.1.3.2 High-Pressure Common Rail System

A high-pressure common rail system with an accumulator type injector and pressurization piston, and the public oil, the oil pressure directly controls injections at higher stress levels (the common rail pressure remains above 100 MPa), fuel injection quantity, and injection timing by electromagnetic control of a three-way valve or a two-way valve to adjust the use of a three-way valve or two-way valve control nozzle change of back pressure in order to change the fuel injection quantity and injection timing.

The main characteristics of the system are:

- (1) There is freedom to adjust the injection pressure (common rail pressure). Using the pressure sensor, detect fuel pressure in the rail, so as to adjust for the oil pump, control the common rail pressure, and adjust the volume of injection.
- (2) With engine speed and throttle opening information, etc., on the basis of optimal fuel injection quantity it is calculated using a computer by controlling the fuel injector solenoid valve moment of electric power and direct control of the fuel injection parameters.

- (3) There is freedom to adjust the injection rate shapes. According to the needs of the engine, set and control the fuel injection rate shape after injection, multistage spray, etc.
- (4) There is freedom to adjust the injection time. According to the parameters such as the engine speed and load, calculate the optimal injection time and control the open and close with the appropriate time, etc., so as to accurately control the fuel injection time.
- (5) It requires a high-pressure fuel pump, as the system components for most of the work are under high pressure and thus may easily fail. Overall, a high-pressure common rail system can be realized in a traditional injection system that cannot otherwise achieve this function.

Its advantages are:

- (1) Wide application fields (for cars and light trucks, each cylinder power can be up to 30 kW, while for heavy trucks and motorcycles and marine diesel engines, every cylinder power needs about 200 kW).
- (2) A higher injection pressure; the current is currently up to 180 MPa and will soon be more than 200 MPa.
- (3) Injection starting point, where the end point of injection can be easily changed.
- (4) It can implement pilot injection and main injection, and after injection can be realized according to the discharge requirements, such as five to seven times that of a multistage injection.
- (5) It has an injection pressure corresponding to the actual working condition. The establishment of the injection pressure is with no interdependent relationship between the fuel injection and the common rail pipe, and is always full of fuel injection at a certain pressure. The fuel injection quantity is determined by computer through calculation, but is less constrained by the other conditions.
- (6) Injection timing and injection pressure are stored in the ECU (MAP) to calculate the characteristic curve of the spectrum; then the electromagnetic valve control is installed on each engine cylinder injector (injection units).

It is because of the advantages of using the high-pressure common rail system that several companies and research institutions at home and abroad are devoting a great effort to its study.

1.2 High-Pressure Common Rail System: Present Situation and Development

1.2.1 For a Common Rail System

In the 1980s research work on the high-pressure common rail system began and in the late 1990s the first generation of common rail system products were introduced.

A typical high-pressure common rail system is mainly composed of a high-pressure pump, electric control, common rail injector tube, current limiter, pressure limiting valve, rail pressure sensor, low pressure pump, filter and fuel tank, and sensors, as shown in Figure 1.3.

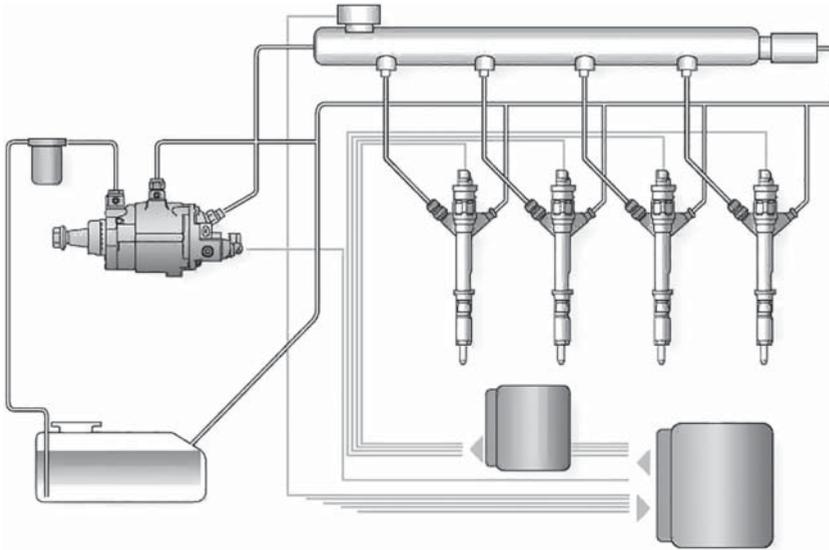


Figure 1.3 The typical schematic of the high-pressure common rail system.

Fuel from the tank passes through at a low pressure to the high-pressure oil pump and then to the radial piston pump, which has three functions: fuel will flow into the high-pressure oil rail, a part of this fuel oil will pass through the injector and is sprayed into the combustion chamber, and a small part will control the injector needle valve after the flow back into the tank. On the high-pressure oil rail there is a pressure sensor; the system will measure the fuel rail pressure compared with the preset value in the ECU, and if the measured value and book value are not consistent, the high-pressure oil rail pressure regulator on the overflow valve will open or close, allowing the fuel back to the fuel tank. Fuel injection timing and fuel quantity control, according to the measured results of each sensor, allow the ECU control high-speed solenoid valve to open and close. The system of the high-pressure oil pump for the three parts of the rotary piston pump has a control input control solenoid valve, when the engine load is low, by closing a feed to reduce the power consumption of the high-pressure oil pump. Fuel injection timing uses the function in the electronic control injector solenoid valve to control the pulse time and the fuel injection quantity uses the function in the electronic control injector solenoid valve to control the pulse width.

Due to the superiority of the high-pressure common rail system, many companies at home and abroad have studied its development and used the characteristics of the common rail system.

1.2.1.1 Germany BOSCH Company of the High-Pressure Common Rail System

So far, BOSCH Company is planning and designing four generations of the high-pressure common rail system. The first-generation batch was on the market in 1997 and with an injection pressure of 135 MPa was mainly used in cars. The second generation of mass production started in 2000, raising the maximum system pressure to 160 MPa, and started using the fuel control function of the high-pressure pump and solenoid valve injector, and improved the injection cycle by pre-injection, main

injection, and many multistage jet injections; it is mainly suitable for engine power under 55 kW/l.

In May 2003, BOSCH Company began to produce innovative piezo inline technology of the third generation of the common rail system. In the first two generations of the common rail system, BOSCH Company mainly paid attention to improve the injection pressure, while the third generation of the common rail system's center of gravity shifted to technical complexity and precision, temporarily to keep the pressure at 160 MPa. The special feature of the third generation of the common rail system is that it uses a fast switch compact piezo inline injector. A piezoelectric actuator is built into the fuel injector on the shaft and is very close to the injector nozzle needle valve. The new fuel injector reduces about 75% of the moving parts and quality. An electromagnetic valve actuator compared the injector of the common rail system, its advantage being: a more accurate supply fuel and injection of the fuel in the combustion chamber, as well as better atomization and mixing. A fuel injector higher switching speed means that the time interval between the two jets is reduced, so the injection process has a more flexible control. The result is that the diesel engine is quieter and the fuel burn is cleaner, more efficient, and gives more engine power. From 2003 to 2008, five years, BOSCH injection pressure of the third generation of the common rail system of the company had two versions in order to achieve the 200 MPa high-pressure jet.

BOSCH Company developed heavy commercial vehicles in the fourth generation of the common rail system. The system configuration of the new type of injector had a pressure conversion device and a pressure transducer that could be triggered independently. Figure 1.4 is a BOSCH fourth-generation N4 interchange type automobile engine high-pressure common rail system. This system has the following characteristics: the system uses two levels of pressurization; in the second level within the fuel injector pressure amplifier, the injection pressure can reach 230–250 MPa; it can realize multiple

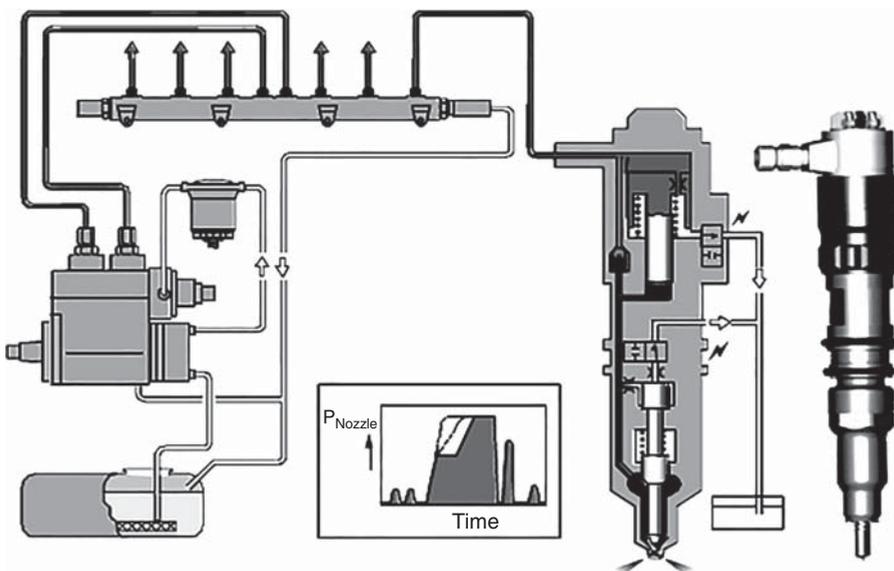


Figure 1.4 BOSCH N4 common rail injector.

injections; the injector with a two-solenoid valve can be used to control the fuel injection rate shape; it is a highly flexible control; and it can make each operation condition point of emission a minimum.

1.2.1.2 The Delphi DCR System of the Company

Delphi is the most representative of the advanced Multec DCR diesel common rail injection systems. The main components of the Multec DCR diesel common rail injection system are a common high-pressure oil rail, high-pressure fuel pressure regulator, ECU for a high-pressure fuel pump, fuel injector, and fuel filter and sensor, etc.

The Multec DCR diesel common rail injection system of injection pressure also has nothing to do with the engine speed and load, for even in low-speed running, the system can still maintain enough pressure for the high-pressure fuel injection. The system can produce injection many times and can meet the requirements of the EU emission regulations although the fuel injector design is unique. Multec DCR mainly adopted a balance control and feedback control strategy of an electric solenoid valve structure of fuel injector, which can provide extremely fast response actions and can accurately measure the fuel flow rate. The quick response, compact structure, small, and exquisite injector solenoid valve control only needs a conventional 12 V car battery drive to work normally. Compared with the world's production of any kind of diesel common rail injection system this system is energy saving, which greatly reduces the production cost of the automobile electronic design system and complexity. The whole system uses a modular design that is easy to apply in different forms and different kinds of engine.

In 2004, a new generation of diesel engine driven directly by the Delphi Company common rail fuel injection system (direct acting diesel common rail (DADCR) system) was introduced into the market. Because the new fuel injector system used piezoelectric actuators, the high-pressure pipe line was not required, which greatly saved the energy waste caused by the high-pressure oil return.

1.2.1.3 Denso High-Pressure Common Rail Injection System of the Company

Denso Co. Ltd. is one of the earliest research and development companies to produce a common rail system, and in 1995 took the lead in the world production of commercial vehicles using the common rail system, the first generation of which entered mass production in 1998. Their product was used in Japan's big four commercial vehicle manufacturing companies. Shortly thereafter, a passenger car using the common rail system began in cooperation and development with Toyota, and in June 1999, production commenced for export of cars to the European market. From that development and experience of the first generation common rail system, the system was further developed to produce the second generation system, with a practical application appearing in June 2002.

The second generation of the common rail system included a fuel injection device where the high-pressure injection was introduced many times with a burning cycle and high-precision injection quantity control, which is critical technology for the development of the second generation of common rail systems focusing on the following two aspects: one is a highest injection pressure of 180 MPa and the second is a high-precision multiple injection capacity.

1.2.2 High-Power Marine Diesel Common Rail System

Relative to the automotive diesel common rail system, the marine diesel common rail system includes new features, mainly including:

- (1) A loop supply of a large amount of oil. Under the condition of a small cycle fuel injection quantity, using the electromagnetic valve can realize accurate control of the fuel injection process. Under the condition of a larger circulation of oil, how can control of the fuel injection process ensure the stability of the system pressure; this needs careful study.
- (2) A large marine diesel engine power requires high system security. If the diesel engine fuel system fails there will be serious consequences, so the system should include very effective safety protection measures.
- (3) As opposed to a relatively stationary diesel engine, in a marine diesel engine the electronic control system electromagnetic interference is stronger, creating a very bad working environment. The narrow space, dampness, corrosive gases such as those produced by environmental conditions of the common rail system signal acquisition, signal processing, electromagnetic compatibility of ECU, etc., make higher requirements necessary.
- (4) The vehicle diesel engine has a vehicle load characteristic and its operation with is by a throttle control. In comparison the load characteristics of the marine diesel engine run as a power plant or as the propulsion characteristics of the host, completely by the ECU control strategy during operation control of the diesel engine speed.
- (5) As used in a marine diesel engine, the fuel quality is worse than for an automotive machine, so the requirements to ensure the fuel system can run reliably an inferior fuel is used under high pressure.

Because the marine diesel engine has the characteristics above, in order to improve system security, common rail pressure fluctuation should be reduced and the characteristics of the marine common rail system need to be adapted with some significant differences made from that of the common rail system.

1.2.2.1 System Structure

A typical marine common rail system is that of L'Orange for the MTU Company MTU8000 series diesel engine production of the common rail system and that of Wartsila Company for Sulzer RTA – flex marine diesel engine production of the common rail system. Figure 1.5 gives the Wartsila ship common rail system schematic diagram (the system can be applied to the 4–18 marine diesel engine cylinder). The whole system consists of a high-pressure oil pump, high-pressure oil rail, accumulator, electronically controlled injector, control oil, electric control system unit, and the composition of the high-pressure oil pipe. The high-pressure oil pump is used to press the fuel into the high-pressure oil rail connecting each accumulator to each other by high-pressure tubing to offer jet fuel to two injectors. Electronically controlled injector fuel is injected and controlled by an electromagnetic valve oil circuit control. L'Orange for MTU Company MTU8000 series diesel engine production of the common rail system and structure of the Wartsila common rail systems are similar, in that in the system each accumulator is only responsible for providing a fuel injector, jet fuel, and fuel injector directly controlled by an electromagnetic valve, without the need of setting

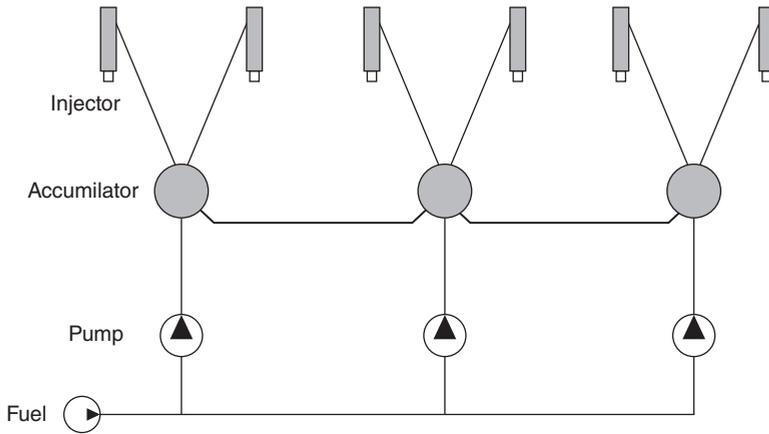


Figure 1.5 Schematic diagram of the Wartsila common rail system.

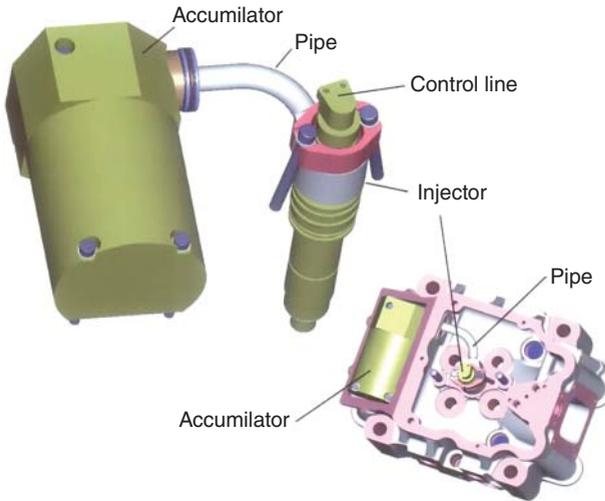


Figure 1.6 MTU8000 injector and accumulator.

up a control hydraulic system to control it. Figure 1.6 shows the accumulator and injector arrangement.

1.2.2.2 High-Pressure Oil Pump

Because the system does not require only high-pressure fuel in the fuel injection stage to be provided, the high-pressure oil pump adopts multiple bumps on the oil supply CAM method, which can effectively reduce the peak torque and improve the high-pressure oil pump volume efficiency. To control the amount of fuel into the accumulator, a high-pressure oil pump inlet is equipped with a rotary solenoid valve to control the oil. Because of the high-pressure oil pump, the oil valve quality has a great influence on the system, so the high-pressure oil pump is used for monitoring the oil valve status of the thermocouple.